

Prepared for:

## Baiada Poultry Pły Limited

20 June 2019
The Transport Planning Partnership

# Oakburn Poultry Processing Plant Road Transport Assessment 

Client: Baiada Poultry Pty Limited

Version: Final
Date: 20 June 2019
TTPP Reference: 18089
Quality Record

| Version | Date | Prepared by | Reviewed by | Approved by | Signature |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Final | $20 / 6 / 19$ | P Dalton | K Hollyoak | P Dalton | Placton |

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## 1 Introduction

This report has been prepared on behalf of Baiada Poultry Pty Limited to present the findings of an assessment of the road transport implications of a new processing plant on the site of its Oakburn rendering plant near Tamworth.

The proposed processing plant would have capacity to process three million birds per week, and the existing rendering plant would increase its production from 120 tonnes per day to 240 tonnes per day of finished product. A new vehicular access would be constructed for the use of staff and deliveries, and the existing access on Oxley Highway retained for visitors and emergency access only.
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## 2 Existing Road Environment

### 2.1 Site Location

The subject site is located at 1154 Gunnedah Road, approximately 9 km west of Tamworth.

### 2.2 Road Network

Oxley Highway forms part of the HW 11 State road link between Port Macquarie in the east and Nevertire in the west, via Tamworth, Gunnedah and Coonabarabran. In the vicinity of the site, Oxley Highway is known as Gunnedah Road, and has a single travel lane in each direction and sealed shoulders. The posted speed limit is $100 \mathrm{~km} / \mathrm{h}$.

The subject site has direct access to Gunnedah Road via a T-intersection. At the intersection, Gunnedah Road is locally widened to provide an auxiliary right turn deceleration and storage lane for vehicles entering the site. The intersection treatment is generally consistent with an Austroads Channelised Right Turn (CHR) treatment in Gunnedah Road, which moves the slower turning vehicles from the through traffic stream.

Through Tamworth, Oxley Highway is also known as Duri Road, Bridge Street, Brisbane Street, and Marius Street. Gunnedah Road crosses the Main Northern Railway just to the west of its intersection with Duri Road, at a road over rail crossing. The intersection of Gunnedah Road and Duri Road is controlled with a roundabout, with bypass lanes for the left turns to and from Gunnedah Road, and for southbound traffic along Duri Road.

Wallamore Road provides a connection between Gunnedah Road west of Tamworth and Manilla Road via Appleby Lane, following the alignment of the West Tamworth Barraba Railway. Wallamore Road has a single travel lane in each direction, typically with dashed centre linemarking or no centre linemarking, and localised widening at major intersections and accesses. Wallamore Road has a posted speed limit of $80 \mathrm{~km} / \mathrm{h}$ west of Kingsford Smith Street.

Goddard Lane is a local road which links Gunnedah Road and Wallamore Road, and has a single travel lane in each direction, with dashed centre linemarking and a wide sealed carriageway. At the intersection of Goddard Lane with Gunnedah Road, an auxiliary right turn (AUR) and auxiliary left turn treatment (AUL) are provided in Gunnedah Road. An acceleration lane is also provided for vehicles exiting Goddard Lane towards Tamworth. RMS is planning improvements to the intersection including a westbound acceleration lane for heavy vehicles (RMS, 2017). The intersection of Goddard Lane with Wallamore Road is a basic rural road intersection.

The state government has provided funding to commence repair and reinstatement of the West Tamworth Barraba Railway from West Tamworth to Westdale, as the first stage of a
larger project to deliver a multi-user Rail Freight Intermodal Terminal, expected to be located near the intersection of Goddard Lane and Wallamore Road.

Goddard Lane provides access to the West Tamworth Glen Artney Industrial Estate, which includes Armstrong Street, Ponda Rosa Road, and Phoenix Street. These roads are each constructed with a wide carriageway and single travel lane in each direction, suitable for use by heavy vehicles.

Bowlers Lane provides a link between Gunnedah Road and Wallamore Road, extending southeast of Gunnedah Road where it is known as Old Winton Road. RMS has recently widened Oxley Highway and improved the intersection between Bowlers Lane and Oxley Highway (RMS, 2017). The intersection of Bowlers Lane with Wallamore Road is a basic rural Tintersection. Bowlers Lane provides access to the Baiada Bowlers Lane Poultry Facilities.

### 2.3 Public Transport

The existing public transport services in the region have been reviewed with regard to the site's accessibility by public transport. Table 2.1 summarises the existing bus and rail services and frequencies in the region, Figure 2.1 presents the bus routes.

Table 2.1: Public Transport Facilities

| Service | Route | Route Description | Site Proximity | Frequency |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Weekday AM | Weekday PM |
| Rail | North Western NSW | Sydney to Armidale | 11.5 km | No service | 1 service |
|  |  | Armidale to Sydney |  | 1 service | No service |
| Bus | 428 | Quirindi to Tamworth | 9.2 km | 3 services | 3 services |
|  | 430 | Oxley Vale via Hospital | 10.8 km | 6 services | 9 services |
|  | 431 | North \& East via Hospital | 10.7 km | 2 services | 3 services |
|  | 433 | South 2 Dibar Drive | 9.2 km | 5 services | 7 services |
|  | 435 | South 1 | 9.2 km | 6 services | 6 services |
|  | 437A | Westdale \& Coledale via Taminda | 5.4 km | 4 services | No service |
|  | 437B | Coledale \& Westdale via Taminda | 5.4 km | No service | 6 services |
|  | 443 | Manilla to Tamworth | 11.5 km | 1 service | 1 service |
|  | 444 | Bendemeer to Tamworth | 11.5 km | Up to 2 services | Up to 2 services |

Figure 2.1: Tamworth Bus Guide Map


The site is not well located to existing public transport services. Bus Route 437 is the closest service to the site, traveling from Tamworth along Gunnedah Road as far as Evans Street at Westdale, over 5 km from the site. Staff or visitors would not rely on existing public transport services to access the site.

### 2.4 Historic Traffic Data

Historic survey data on roads of relevance to the site operations has been collated from surveys conducted during July 2015. Key results for average weekday conditions are summarised in Table 2.2.

Table 2.2: Surveyed Weekday Average Traffic Volumes 2015

| Road and Location | AM Peak Hour |  | PM Peak Hour |  | Vehicles per Day |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Hour Start | Vehicles per Hour | Hour Start | Vehicles per Hour |  |
| Jewry Street West of Wirraway Street | 8:00 | 961 | 15:00 | 1,027 | 11,399 |
| Bridge Street <br> At Peel River Bridge | 8:00 | 1,916 | 15:00 | 2,172 | 24,464 |
| Oxley Highway East of Edith Street | 8:00 | 961 | 15:00 | 1,152 | 12,837 |
| Oxley Highway East of Evans Street | 9:00 | 618 | 15:00 | 815 | 8,115 |
| Oxley Highway <br> North of Goddard Lane | 8:00 | 337 | 15:00 | 377 | 4,256 |
| Oxley Highway South of Byamee Lane | 8:00 | 278 | 16:00 | 305 | 3,469 |
| Oxley Highway <br> North of Joshua Street | 8:00 | 247 | 16:00 | 293 | 3,141 |

The results in Table 2.2 demonstrate the extent to which traffic volumes decline to the west along Oxley Highway, with some 9,368 fewer vehicles per day on Oxley Highway near Byamee Lane (approximately 12 km west of Duri Road) than near Duri Road.

### 2.5 Traffic Volume Surveys

To quantify existing traffic conditions on roads of relevance to the proposed development, automatic tube count surveys were commissioned at the following locations, which are presented on Figure 2.2, which includes the aforementioned 2015 survey locations:

- Oxley Highway, north of the site access;
- Oxley Highway, south of Goddard Lane;
- Wallamore Road, south of Goddard Lane;
- Manilla Road, south of Browns Lane;
- New England Highway, south of Hall Street;
- Gunnedah Road, east of Edith Street;
- Duri Road, south of Bylong Road; and
- Goonoo Goonoo Road, north of Burgmanns Lane.

Figure 2.2: Survey Data Locations


The surveys were conducted between Wednesday 27 June and Tuesday 3 July 2018. Key results for average weekday conditions are summarised in Table 2.3.

Table 2.3: Surveyed Weekday Average Traffic Volumes 2018

| Road and Location | AM Peak Hour |  | PM Peak Hour |  | Vehicles per Day | Percent Heavy (\%) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Hour Start | Vehicles per Hour | Hour Start | Vehicles per Hour |  |  |
| Oxley Highway <br> North of Baiada Access | 8:00 | 304 | 16:00 | 341 | 3,963 | 18.3 |
| Oxley Highway South of Goddard Lane | 8:00 | 305 | 15:00 | 483 | 5,040 | 17.3 |
| Wallamore Road South of Goddard Lane | 8:00 | 270 | 15:00 | 438 | 4,033 | 16.0 |
| Manilla Road South of Browns Lane | 8:00 | 390 | 16:00 | 400 | 4,443 | 9.4 |
| New England Highway South of Hall Street | 8:00 | 1,057 | 16:00 | 1,098 | 12,106 | 9.8 |
| Duri Road South of Bylong Road | 8:00 | 366 | 16:00 | 358 | 4,102 | 17.8 |
| Goonoo Goonoo Road North of Burgmanns Lane | 8:00 | 548 | 17:00 | 570 | 6,793 | 15.3 |
| Appleby Lane East of Oxley Highway | 7:00 | 48 | 16:00 | 51 | 535 | 21.2 |

The survey results demonstrate that the morning peak hour typically occurs between 8:00 am and 9:00 am, while the afternoon peak hour occurs at different times at the various locations. Close to the industrial area, the afternoon peak hour occurs between 3:00 pm and $4: 00 \mathrm{pm}$, and on the outskirts of Tamworth, the peak hour tends to occur from 4:00 pm to 5:00 pm.

### 2.6 Intersection Surveys

Intersections are typically the critical locations in the road network, due to the need for opposing movements to occupy the same space. To quantify existing intersection conditions, a program of peak period intersection turning movement surveys was commissioned by TTPP at the intersections of:

- Oxley Highway and site access;
- Oxley Highway and Goddard Lane;
- Goddard Lane and Armstrong Street;
- Goddard Lane and Wallamore Road;
- Oxley Highway and Duri Road;
- Oxley Highway, Marius Street and Brisbane Street; and
- Peel Street and Jewry Street.

The survey locations are presented in Figure 2.2. The surveys were conducted between 6 am and 10 am , and between 3 pm and 7 pm on Wednesday 27 June, 2018. The time of the busiest hour at each intersection varied across the surveyed intersections, with the morning peak hour typically starting between 7.45 am and 8.15 am , and the evening peak hour starting between 3.00 pm and 3.45 pm . The peak hours identified below are the hour during which the highest number of vehicles passed through each intersection.

Table 2.4: Surveyed Peak Hour Vehicle Movements at Intersections (vehicles per hour)

| Intersection | AM Peak Hour |  |  |  | PM Peak Hour |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Hour Start | Light | Heavy | Total | Hour Start | Light | Heavy | Total |
| Oxley Highway and Baiada Access | 7:45 | 278 | 53 | 331 | 15:15 | 313 | 57 | 370 |
| Oxley Highway and Goddard Lane | 7:45 | 356 | 87 | 443 | 15:15 | 550 | 75 | 625 |
| Goddard Lane and Armstrong Street | 7:45 | 201 | 53 | 254 | 15:15 | 355 | 44 | 399 |
| Goddard Lane and Wallamore Road | 8:00 | 240 | 58 | 298 | 15:30 | 444 | 42 | 486 |
| Oxley Highway and Duri Road | 8:00 | 1,442 | 109 | 1,551 | 15:15 | 1,638 | 111 | 1,749 |
| Oxley Highway and Marius Street | 8:15 | 1,785 | 128 | 1,913 | 15:00 | 1,982 | 114 | 2,096 |
| Peel Street and Jewry Street | 8:15 | 2,509 | 169 | 2,678 | 15:45 | 2,773 | 123 | 2,896 |

The intersection surveys demonstrate that the evening peak hourly traffic volumes are typically higher than the morning peak hourly volumes.

### 2.7 Road Network Performance

The Austroads (2017) Guide to Traffic Management Part 3: Traffic Studies and Analysis provides guidelines for the capacity and performance of two lane, two-way rural roads, which in turn, refers to the Highway Capacity Manual (HCM) (Transportation Research Board, 2016).

The capacity of a road is defined as the maximum hourly rate at which vehicles can reasonably be expected to traverse a point or uniform section of a lane or roadway during a given time period under the prevailing roadway, traffic and control conditions. The capacity of a single traffic lane will be affected by factors such as the pavement width and restricted lateral clearances, the presence of heavy vehicles and grades.

Level of Service (LOS) is defined as a qualitative measure describing the operational conditions within a traffic stream as perceived by drivers and/or passengers. A LOS definition generally describes these conditions in terms of factors such as speed and travel time, freedom to manoeuvre, traffic interruptions, comfort, convenience and safety. LOS A provides the best traffic conditions, with no restriction on desired travel speed or overtaking.

LOS B to D describes progressively worse traffic conditions. LOS E occurs when traffic conditions are at or close to capacity, and there is virtually no freedom to select desired speeds or to manoeuvre in the traffic stream. The service flow rate for LOS E is taken as the capacity of a lane or roadway. In rural situations, LOS C is generally considered to be acceptable. At LOS C, most vehicles are travelling in platoons, and travel speeds are curtailed. At LOS D, platooning increases significantly, and the demand for passing is high, but the capacity to do so is low.

The LOS experienced by drivers on two-way rural roads is dependent on the drivers' expectations regarding the road, and three classes of road are defined in the HCM. Class I roads are those on which motorists expect to travel at relatively high speeds. They most often serve long-distance trips or provide connecting links between facilities that serve longdistance trips. Class II roads are those on which motorists do not necessarily expect to travel at high speeds, and may function as access routes to Class I facilities, serve as scenic or recreational routes or pass through rugged terrain. Class III roads serve moderately developed areas, and may be portions of a Class I or Class II highway that pass through small towns or developed recreational areas, where local traffic mixes with through traffic, and the density of unsignalised roadside access points increases.

On Class I roads, LOS is defined in terms of Percent Time Spent Following (PTSF) and Average Travel Speed (ATS). On Class II roads, LOS is defined only in terms of PTSF. The PTSF is a measure of the level of opportunities to overtake, and is estimated from the demand traffic volumes, the directional distribution of that traffic, and the percentage of no-passing zones.

On Class III roads, LOS is defined in terms of Percent of Free-Flow Speed (PFFS), which is the ratio of ATS to the free-flow speed, representing the ability of vehicles to travel at or near the posted speed limit. The LOS criteria for two lane roads are as shown in Table 2.5, noting that the HCM defines ATS in miles per hour ( $\mathrm{mi} / \mathrm{h}$ ).

Table 2.5: LOS Criteria for Class I and Class II Two Lane Roads

| LOS | Class I |  | Class II | Class III |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | PTSF (percent) | ATS (mi/h)A | PTSF (percent) | PFFS (percent) |  |  |
| A | $\leq 35$ | $\geq 55$ | $\leq 40$ | $>91.7$ |  |  |
| B | $>35-50$ | $>50-55$ | $>40-55$ | $>83.3-91.7$ |  |  |
| C | $>50-65$ | $>45-50$ | $>55-70$ | $>75.0-83.3$ |  |  |
| D | $>65-80$ | $>40-45$ | $>70-85$ | $>66.7-75.0$ |  |  |
| E | $\geq 80$ | $\leq 40$ | $\leq 66.7$ |  |  |  |
| F | Demand exceeds capacity |  |  |  |  |  |

A note that $1 \mathrm{mi} / \mathrm{h}$ is equivalent to approximately $1.6 \mathrm{~km} / \mathrm{h}$
The primary determinant of a road's classification for operational analysis is the drivers' expectations, which may not necessarily agree with the functional classification. The surveyed location on Oxley Highway north of the rendering plant access would typically be considered as a Class II road under the HCM descriptions, as drivers would expect some level
of restriction to their freedom of movement along the routes as a result of characteristics of the route such as limits on the opportunities for overtaking (e.g. centre line marking, sight distances, lack of overtaking lanes) and proximity to Tamworth and the industrial areas. The other surveyed locations are within built up areas, where the performance of intersections is likely to be the main constraint on vehicle movements, and so have not been considered using this methodology. Intersection operating conditions are discussed in Section 2.8. The surveyed location south of Goddard Lane has been assessed using the HCM method, although the operation of intersections are considered the more likely constraint.

Table 2.6 summarises the Levels of Service on Oxley Highway based on the surveyed average weekday peak hour conditions. The results demonstrate that the existing levels of service experienced by drivers on Oxley Highway are satisfactory, with low levels of interference to travel. It is noted that should the surveyed locations on Oxley Highway be considered as Class I roads, the resulting levels of service would also be satisfactory.

Table 2.6: Surveyed Weekday Peak Hour Midblock Performance

| Road and Location | Class | Inbound to <br> Rendering Plant |  | Outbound from <br> Rendering Plant |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | PTSF | LOS | PTSF | LOS |
| Oxley Highway North of Site Access |  |  |  |  |  |
| AM Peak Hour | $\\|$ | 45.1 | B | 32.8 | A |
| PM Peak Hour | $\\|$ | 45.7 | B | 43.8 | B |
| Oxley Highway South of Goddard Lane |  |  |  |  | A |
| AM Peak Hour | $\\|$ | 26.5 | A | 26.7 | B |
| PM Peak Hour | $\\|$ | 33.8 | $A$ | 41.5 |  |

### 2.8 Intersection Operation

The operating characteristics of the surveyed intersections have been assessed using SIDRA INTERSECTION 8, an analysis program which determines characteristics of intersection operating conditions including the degree of saturation, average delays, and levels of service. The degree of saturation, or x-value, is the ratio of the arrival rate of vehicles to the capacity. The average delay, expressed in seconds per vehicle, is measured over all movements at signalised intersections, and over the movement with the highest average delay at roundabout and priority intersections. Average vehicle delay is the commonly used measure of intersection performance defined by RMS. Table 2.7 shows the criteria adopted by RMS for assessing the level of service.

Table 2.7: Intersection Level of Service Criteria

| Level of Service (LoS) | Average Delay per vehicle (secs/veh) | Traffic Signals, Roundabout | Give Way \& Stop Sign |
| :---: | :---: | :---: | :---: |
| A | Less than 14 | Good operation | Good operation |
| B | 15 to 28 | Good with acceptable delays and spare capacity | Acceptable delays and spare capacity |
| C | 29 to 42 | Satisfactory | Satisfactory, but accident study required |
| D | 43 to 56 | Near capacity | Near capacity, accident study required |
| E | 57 to 70 | At capacity, at signals incidents will cause excessive delays | At capacity, requires other control mode |
| F | Greater than 70 | Extra capacity required | Extreme delay, major treatment required |

Table 2.8 presents a summary of the existing peak hour operating characteristics of the surveyed intersections. These peak hours represent the hour during which the highest number of vehicles passed through each intersection (refer to Table 2.4).

Table 2.8: Existing Peak Hour Intersection Operating Conditions (2018)

| Intersection | AM Peak Hour |  |  | PM Peak Hour |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
|  | X-Value | Average <br> Delay | LoS | X-ValueDelaye <br> Dela | LoS |  |
| Oxley Highway and <br> Site Access | 0.10 | 8.1 | A | 0.11 | 9.6 | A |
| Oxley Highway and <br> Goddard Lane | 0.13 | 10.8 | A | 0.22 | 11.7 | A |
| Goddard Lane and <br> Armstrong Street | 0.11 | 8.2 | A | 0.10 | 8.4 | A |
| Goddard Lane and <br> Wallamore Road | 0.14 | 8.6 | A | 0.28 | 9.5 | A |
| Oxley Highway and <br> Duri Road | 0.35 | 11.5 | A | 0.30 | 10.5 | A |
| Oxley Highway and <br> Marius Street | 0.69 | 29.4 | C | 0.72 | 34.3 | C |
| Peel Street and <br> Jewry Street | 0.77 | 16.5 | A | 0.87 | 18.5 | B |

On the basis of the above assessment results and observations of operating conditions during the peak hour periods, it is evident that the intersections currently operate at good levels of service, with spare capacity and short average delays.

It is noted that at the roundabout at the intersection of Peel Street and Jewry Street, the geometry of the roundabout allows vehicles to turn left from Jewry Street to Peel Street and from Peel Street to Jewry Street without being in conflict with circulating or exiting traffic in the roundabout, as there is only a single circulating lane past those approaches.

The circulating vehicles would generally travel from the circulating lane to the right hand of the two exiting lanes, allowing vehicles to turn into the left hand exiting lane unopposed. The line marking of the roundabout is however unclear and observations suggest that drivers tend to wait to give way to those vehicles exiting the roundabout, although this is not always the case. The results in Table 2.8 reflect the assumption that the left turning drivers give way to all circulating and exiting traffic, and tend to overestimate the delays and queues which result. With minor amendments to line marking, the capacity of the roundabout would be increased, particularly with regard to the capacity for the left turn movements.

### 2.9 Road Safety

Validated crash data was obtained from the RMS for the most recent five year period available, being from 1 July 2012 to 30 June 2017. The data includes those crashes which conform to the national guidelines for reporting and classifying road vehicles crashes based on the following criteria:

- The crash was reported to the police.
- The crash occurred on a road open to the public.
- The crash involved at least one moving vehicle.
- The crash involved at least one person being killed or injured or at least one motor vehicle being towed away.

Crash data was reviewed for primary access routes for the site, including:

- Appleby Lane;
- Oxley Highway, from west of Appleby Lane to Duri Road;
- Oxley Highway, between Duri Road and Marius Street;
- Wallamore Road, between Appleby Lane and Jewry Street/Dampier Street;
- Goddard Lane;
- Duri Road, between Oxley Highway and Burgmanns Lane;
- Burgmanns Lane;
- Dampier Street - Jewry Street;
- Ebsworth Street;
- Manilla Road - Peel Street - Darling Street - Marius Street, between Bridge Street and Oxley Vale; and
- Marius Street, between Bridge Street and Crawford Street.

Table 2.9 presents a summary of the general crash types reported on the access routes described above.

Table 2.9: General Crash Types on Site Access Routes (1 July 2012 to 30 June 2017)

| Access Route |  | Multiple Vehicles |  |  |  |  | Single Vehicle |  |  |  | 흥 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & \text { 들 } \\ & \text { 은 } \\ & \frac{1}{0} \\ & 0 \end{aligned}$ |  |  |  |  | $\begin{aligned} & \text { 인 } \\ & \text { 든 } \\ & \text { 뭉 } \\ & 00 \end{aligned}$ | $\begin{aligned} & \text { 등 } \\ & \text { ᄃ } \end{aligned}$ |  |  |  |  |
| Appleby Lane | - | - | - | - | - | - | - | 1 | - | - | 1 |
| Oxley Highway Appleby Lane to Duri Road | - | 7 | 3 | 12 | - | - | 2 | 11 | 2 | - | 37 |
| Oxley Highway Duri Road to Marius Street | - | 12 | 11 | 16 | 4 | - | - | 5 | 2 | - | 50 |
| Wallamore Road | - | 1 | 3 | 1 | - | - | 1 | 3 | 2 | - | 11 |
| Goddard Lane | - | 1 | - | - | - | - | - | - | - | - | 1 |
| Duri Road | 2 | 5 | - | 3 | 1 | - | - | 8 | 4 | - | 23 |
| Burgmanns Lane | - | - | - | - | - | - | - | - | - | - | - |
| Dampier Street-Jewry Street | - | - | 1 | 9 | - | - | - | 2 | - | - | 12 |
| Ebsworth Street | - | 1 | - | 3 | - | - | - | 1 | 1 | - | 6 |
| Manilla Road | - | 12 | - | 9 | 1 | - | 1 | 4 | 1 | - | 28 |
| Marius Street | - | 2 | 4 | 10 | 1 | - | - | 2 | 2 | - | 22 |

Detailed assessments of crash types and characteristics on each route are presented in Appendix B. Some key findings for each route are summarised below.

## Appleby Lane

One crash occurred on Appleby Lane over the five years investigated. A westbound station wagon left the carriageway to the right and struck a tree or bush. This occurred at 5:30 am on 3 March 2013, in fine weather on a wet road surface.

## Oxley Highway - Appleby Lane to Duri Road

- One fatal crash occurred on 31 March 2017, in which a northbound car travelled on the wrong side of the road and struck a southbound 4WD head on in a $100 \mathrm{~km} / \mathrm{h}$ speed limit zone. The crash occurred mid-afternoon in fine weather and on a dry road surface. Fatigue was nominated as a contributing factor to the crash.
- Approximately 80 percent of the crashes occurred in fine weather and/or on a dry road surface.
- Approximately half of the crashes occurred at intersections.
- Ten of the 37 crashes involved a heavy vehicle as the key vehicle, with half of those being single vehicle crashes.
- Approximately one-third of crashes occurred in $100 \mathrm{~km} / \mathrm{h}$ speed limit areas, which make up around three-quarters of the route investigated.
- No crashes occurred at or near the intersection of Oxley Highway (Gunnedah Road) with the existing Baiada rendering plant site access.
- One crash occurred at the intersection of Oxley Highway and Goddard Lane, in which a station wagon turning right from Goddard Lane struck an eastbound car in Oxley Highway. This occurred at 7:05 am on 12 August 2016 I fine weather on a dry road surface.
- $\quad$ Speed was nominated as a contributing factor in two crashes, and fatigue was nominated as a contributing factor in five crashes. With one exception (being the fatal crash referred to earlier) all these were single vehicle crashes.

It is noted that significant upgrading of Oxley Highway between Duri Road and Cole Road occurred during the period under review, including construction of roundabouts and median turning treatments during 2014-15. The frequency of crashes on this route has declined over that period, from 16 crashes in the first 18 months of the period reviewed to 10 crashes in the most recent 18 months of the period reviewed.

## Oxley Highway - Duri Road to Marius Street

- Approximately 90 percent of the crashes occurred in fine weather and/or on a dry road surface.
- Nearly 90 percent of the reported crashes occurred at intersections (under priority or roundabout control), with approximately half of those occurring at cross intersections and one third at roundabouts.


## Wallamore Road

One crash occurred at the intersection of Goddard Lane and Wallamore Road, in which a northbound car left the wet carriageway and struck a drain/culvert at 5:03 am. No contributing factors were nominated. The carriageway where this crash occurred has since been upgraded.

## Goddard Lane

One crash occurred on Goddard Lane over the five year period investigated. It occurred at 1:15 am on 4 July 2012 at the intersection with Armstrong Street, in fine weather on a dry road surface. A car turning right out of Armstrong Street struck a northeast-bound utility in Goddard Lane.

## Duri Road - Burgmanns Lane

- Nearly 90 percent of the reported crashes occurred in fine weather or on a dry road surface.
- Two crashes involved pedestrians, one at the intersection of Duri Road with Roberts Street (roundabout), and one on Burgmanns Lane.
- Approximately two-thirds of the crashes occurred at intersections, under either roundabout or priority control.
- Four of the 23 crashes involved a heavy vehicle as the key vehicle, with half of those being single vehicle crashes.


## Dampier Street - Jewry Street

- Three-quarters of the 12 reported crashes were multiple vehicle crashes involving vehicles travelling in the same direction, such as rear end, side swipe or lane changing crashes.
- One crash involved vehicles travelling in opposing directions, at the intersection of Dampier Street with Wallamore Road.


## Ebsworth Street

- Half of the six reported crashes were multiple vehicle crashes involving vehicles travelling in the same direction, such as rear end, side swipe or lane changing crashes.
- One crash involved vehicles travelling in adjacent directions, at the intersection of Ebsworth Street with Plain Street.


## Manilla Road

- Nearly 80 percent of the 28 reported crashes were multiple vehicle crashes, of which more than half involved vehicles travelling in adjacent directions at intersections.
- Six crashes were single vehicle crashes, all of which involved light vehicles.
- Approximately 80 percent of the reported crashes occurred in fine weather and/or on a dry road surface.


## Marius Street

- Approximately three-quarters of the 22 reported crashes were multiple vehicle crashes, of which 60 percent involved vehicles travelling in the same directions, such as rear-end, side swipe or lane change crashes.
- Four crashes were single vehicle crashes, including one motorcycle, one car, one articulated vehicle and one unknown vehicle type.
- Approximately 90 percent of the reported crashes occurred in fine weather and/or on a dry road surface.
transport planning


## 3 Site Operations

### 3.1 Existing Rendering Plant Operations

The existing rendering plant produces 120 tonnes of finished product per day. It employs 21 workers, who work across three shifts. The morning shift employs nine people working from 7:00 am to 3:00 pm, the afternoon shift employs six people between 3:00 pm and 11:00 pm, and the night shift employs six people between 11:00 pm and 7:00 am.

The site has its vehicular access via a T-intersection on Oxley Highway. This access is used by all vehicles accessing the site, including deliveries, staff and visitors. Car parking is currently provided on site for 14 cars.

### 3.2 Existing Traffic Generation and Distribution

### 3.2.1 Deliveries and Dispatch Heavy Vehicles

## Rendering Raw Material

Baiada has confirmed that the rendering plant receives up to 29 trucks per day carrying between 3 tonnes and 40 tonnes, generating 58 trips per day. The delivery trips occur throughout the day and night. Based on the sources of these trips, the likely approach and departure routes of the delivery trucks have been estimated. Of the 58 trucks trips per day, it would be expected that on average:

- 6 trips are on Oxley Highway west, of which;
- 2 trips are via Manilla Road, Wallamore Road and Appleby Lane; and
- 4 trips are via Gunnedah.
- 56 trips are on Oxley Highway east, of which;
- 2 trips are to/from Country Road hatchery south of Oxley Highway;
- 32 trips are to/from Out Street processing plant at West Tamworth;
- 4 trips are through Tamworth via New England Highway north; and
- 18 trips are through Tamworth via New England Highway south.


## Finished Rendered Material

The rendering plant output generates four trucks per day, generating eight trips per day, primarily using B-doubles. These trucks travel to Sydney, Newcastle, Brisbane and Bathurst. Transport of finished materials occurs throughout the day and night. While a small number would travel to and from the east to Tamworth, of the eight trucks trips per day, it would be expected that on average, all trips are on Oxley Highway west of the rendering plant.
transport planning

## General Deliveries and Waste Collection

General deliveries of consumables such as LPG gas and collection of waste generates two trucks per day, generating four vehicle trips per day. Delivery and waste collection vehicles which vary between small rigid trucks, large rigid trucks and semitrailers, and are typically limited to daytime business hours. All of these trips are made between the rendering plant and Tamworth, and so would approach on Oxley Highway east of the site.

### 3.2.2 Staff Light Vehicles

Given that the site's accessibility to public transport is poor, it is expected that existing staff all travel by private vehicle. Some car pooling between staff would occur, and Baiada has advised that typically the staff travel in 15 cars. On this basis the existing staff generate 30 light vehicle trips per day. The majority of staff reside in Tamworth, thus of the 30 existing staff vehicle trips per day, it would be expected that:

- 2 trips are on Oxley Highway west; and
- 28 trips are on Oxley Highway east.

It is assumed that some staff travelling to and from North Tamworth travel via Jewry Street and Dampier Street, while the rest travel on Gunnedah Road to Duri Road/Bridge Street and spread throughout Tamworth.

The distribution of staff trips through the day is related to the shift times operating at the rendering plant, with staff arriving prior to commencement of their shift and departing after completion of their shift.

### 3.2.3 Total Existing Rendering Plant Vehicle Trips

The number of vehicle trips generated by the existing rendering plant has been estimated from the information presented above, and is summarised in Figure 3.1, noting that a trip is a one way movement, a vehicle arriving then departing generates two vehicle trips.

Figure 3.1: Existing Rendering Plant Hourly Traffic Generation (vehicles per hour)


The peak hourly vehicle trip generation of the existing rendering plant is therefore estimated at approximately 11 vehicles per hour in the mid-afternoon, with a lower peak in the morning of approximately eight vehicles per hour.

The estimated average daily distribution of the vehicle trips generated by the existing rendering plant are summarised in Table 3.1.

Table 3.1: Existing Daily Rendering Plant Traffic Distribution Summary (vehicles per day)

| Location | Light Vehicle Trips | Heavy Vehicle Trips | Total Vehicle Trips |
| :--- | :---: | :---: | :---: |
| Rendering Plant <br> Access Road | 30 | 70 | 100 |
| Oxley Highway <br> West of Rendering Plant | 2 | 10 | 12 |
| Appleby Lane <br> North of Oxley Highway | 0 | 2 | 2 |
| Oxley Highway <br> East of Rendering Plant | 28 | 60 | 88 |
| Country Road <br> South of Oxley Highway | 6 | 2 | 2 |
| Jewry Street <br> North of Wallamore Road | 12 | 20 | 6 |
| Duri Road <br> South of Gunnedah Road | 10 | 38 | 32 |
| Bridge Street <br> North of Gunnedah Road | 10 | 6 | 40 |
| Bridge Street <br> North of Out Street | 6 | 2 | 2 |

A trip is a one way movement, a vehicle arriving then departing generates two vehicle trips on the road network

### 3.3 The Proposed Development

Baiada Poultry Pty Limited proposes to build a new processing plant on the subject site. The processing plant would have capacity to process up to three million birds per week, which represents an increase from the approved facility which would have capacity for one million birds per week. The existing rendering plant located within the site would also increase its production level from 120 tonnes of finished product per day to 240 tonnes of finished product per day.

A new vehicular access is proposed to be constructed, with a new driveway connecting to Armstrong Street via Workshop Lane. The new access would be used by all staff and heavy vehicles. The existing access to Gunnedah Road would be retained for the use of visitors only and for emergency access.

### 3.4 Future Operational Traffic Generation and Distribution

### 3.4.1 Deliveries and Dispatch Heavy Vehicles

The number and types of heavy vehicles expected to be generated by the proposed processing plant has been estimated by Baiada as shown in Table 3.2.

Table 3.2: Proposed Processing Plant Daily Heavy Vehicle Trip Generation

| Movement Type | Type of Vehicle | Trucks per Day | Trips per Day |
| :---: | :---: | :---: | :---: |
| Finished Product Dispatch | B-double | 84 | 168 |
| Rendering Raw Material | Large rigid or <br> semitrailer | 70 | 140 |
| Finished Rendered Material | Semitrailer or <br> B-double | 20 | 40 |
| General deliveries and waste collection | Small rigid, large rigid <br> or semitrailer | 20 | 40 |
| Total | 204 | 408 |  |

A trip is a one way movement, a truck arriving then departing generates two vehicle trips

## Live Birds Deliveries

The delivery of live birds to the processing plant would occur between 2:00 am and 6:00 pm. Trucks delivering live birds would be drawn from all directions, thus it is assumed the 168 truck trips per day would be distributed with:

- 84 trips to/from west on Oxley Highway; and
- 84 trips to/from east on Oxley Highway.


## Finished Product Dispatch

Approximately 90 per cent of finished product dispatch vehicles would travel to the west to Gunnedah, then south to other destinations. Dispatch of finished product would occur throughout the day and night. The 140 truck trips generated by dispatch of finished product would be distributed with:

- 14 trips to/from west on Oxley Highway; and
- 126 trips to/from east on Oxley Highway.


## Rendering Raw Material

With the processing plant, the number and distribution of trucks delivering raw material for the rendering plant would alter. The Out Street processing plant at West Tamworth which currently delivers to the rendering plant would be closed, and the proposed on-site processing plant would replace the need for those deliveries. The rendering plant would receive some 20 trucks per day, generating 40 trips per day. Based on the sources of these trips, the likely approach and departure routes of the 40 delivery truck trips per day have been estimated as:

- 10 trips to/from west on Oxley Highway; and
- 30 trips to/from east on Oxley Highway, of which:
- 4 trips are to/from Country Road hatchery south of Oxley Highway;
transport planning
- 26 trips are through Tamworth via New England Highway south.


## Finished Rendered Material

The rendering plant output is expected to generate eight to ten trucks per day, generating up to 20 trips per day, primarily using B-doubles. The finished rendered material delivery trips would occur throughout the day and night. These trucks would travel to destinations destinations as the existing rendering plant dispatch trips, with 90 per cent travelling to and from the site via Gunnedah. Of the 20 truck trips per day, it would be expected that all trips would be to/from the east site, with:

- 18 trips to/from the west on Oxley Highway; and
- 2 trips to/from the east on Oxley Highway.


## General Deliveries and Waste Collection

General deliveries of consumables and collection of waste would typically be limited to daytime business hours. The significant majority of the forecast 40 truck trips per day would be made between the site and Tamworth, and so would be expected to approach and depart on Oxley Highway east of the site.

### 3.4.2 Staff Light Vehicles

The proposed processing facility would operate for 24 hours a day, seven days a week. Shift start and end times would however vary for workers in different parts of the facility. Based on attendance data at its Hanwood Processing Plant, Baiada has estimated the number of staff expected to be present at the site throughout a typical day/night. This is considered an overestimate of total staff numbers, as some efficiencies would result with the new facility compared with current operations at Hanwood. This data is presented in Table 3.3. The nominal start and end times presented in Table 3.3 generally represent the earliest start time that employees would start working that shift, and the latest end time that employees would conclude that shift. Operationally, staff working hours are typically spread over the time ranges given, with actual numbers on site at any one time being dependent upon current production.

Table 3.3: Proposed Processing Plant Staff Attendance

| Shift | Number of Staff | Nominal Start Time | Nominal End Time |
| :---: | :---: | :---: | :---: |
| Line 1 Live Birds | 100 | 0:00 | 12:00 |
| Line 2 Live Birds | 100 | 6:00 | 19:00 |
| Line 1 Processing (Day) | 165 | 4:00 | 15:00 |
| Line 2 Processing (Day) | 165 | 4:00 | 15:00 |
| Line 1 Processing (Afternoon) | 165 | 14:00 | 1:00 |
| Line 2 Processing (Afternoon) | 165 | 14:00 | 1:00 |
| Tray Pack (Day) | 100 | 4:00 | 15:00 |
| Tray Pack (Afternoon) | 100 | 13:00 | 1:00 |
| Rendering (Morning) | 9 | 6:00 | 15:00 |
| Rendering (Afternoon) | 6 | 14:00 | 23:00 |
| Rendering (Night) | 6 | 22:00 | 7:00 |
| Administration | 65 | 7:00 | 18:00 |
| Loading Dock (Day) | 15 | 6:00 | 15:00 |
| Loading Dock (Night) | 15 | 15:00 | 6:00 |

Staff would be drawn primarily from the local Tamworth area, with an estimated 95 percent of staff travelling to and from the east of the processing facility. Car pooling would be expected to occur, noting that the existing rendering plant staff travel with an average of 1.4 people per vehicle. For the purpose of this assessment, a lower average car occupancy of 1.2 people per vehicle has been applied, based on TTPP's experience of similar developments which operate 24 hours per day in regional locations.

On this basis, the staff would be expected to generate up to 1,966 vehicle trips per day on the road network (being 983 inbound and 983 outbound trips). With the majority of staff expected to reside in Tamworth, of the total staff trips, it would be expected that:

- 98 trips (5 per cent) would be to and from the west and north-west; and
- 1,868 trips ( 95 per cent) would be to and from the east.

It is assumed that some staff travelling to and from North Tamworth travel via Jewry Street while the rest travel on Oxley Highway to Duri Road/Bridge Street and spread throughout Tamworth.

The distribution of staff trips through the day is related to the proposed shift times operating at the rendering plant, with staff arriving prior to commencement of their shift and departing after completion of their shift, including an allowance for the spread of shift start times within the nominal shift times presented in Table 3.3.

### 3.4.3 Total Processing Plant Traffic Generation

Figure 3.2 presents the estimated spread of vehicle trips expected to be generated by the proposed processing plant, noting that a trip is a one way movement, a vehicle arriving then departing generates two vehicle trips.

Figure 3.2: Processing Plant Hourly Traffic Generation (vehicles per hour)


Figure 3.2 suggests that the busiest periods for traffic generation of the proposed processing plant would occur in the early afternoon, with up to 358 vehicle trips per hour between 2:00 pm and $3: 00 \mathrm{pm}$, and in the middle of the night, with up to 238 vehicle trips per hour between midnight and 1:00 am.

The typical on-street peak hours on road serving the site occur between 8:00 am and 9:00 am, and between 4:00 pm and 5:00 pm (refer to Table 2.3 and Table 2.4). At these times, the expected traffic generation of the processing plant is low, at 19 and 24 heavy vehicle trips per hour respectively, as staff would not be arriving or departing at those times.

### 3.5 New Vehicle Access via Armstrong Street

The processing plant is proposed to have its access via Armstrong Street and Goddard Lane. Vehicles travelling to and from the site would therefore be able to travel via either Oxley Highway or Wallamore Road to access Goddard Lane. Table 3.4 summarises the estimated distribution of traffic generated by the proposed processing plant on the road network over
the average day. This conservatively assumes that all heavy vehicles to and from the west and north-west would continue to use Appleby Lane and/or Oxley Highway to access the site rather than Wallamore Road.

Table 3.4: Proposed Processing Plant Traffic Distribution Summary (vehicles per day)

| Location | Light Vehicle Trips | Heavy Vehicle Trips | Total Vehicle Trips |
| :---: | :---: | :---: | :---: |
| Processing Plant Access Road | 1,966 | 408 | 2,374 |
| Armstrong Street <br> West of Goddard Lane | 1,966 | 408 | 2,374 |
| Goddard Lane <br> North of Oxley Highway | 1,178 | 408 | 1,586 |
| Goddard Lane South of Wallamore Road | 788 | 0 | 788 |
| Oxley Highway <br> West of Goddard Lane | 58 | 124 | 182 |
| Appleby Lane <br> North of Oxley Highway | 0 | 64 | 64 |
| Oxley Highway West of Appleby Lane | 58 | 60 | 118 |
| Oxley Highway <br> East of Goddard Lane | 1,120 | 284 | 1,404 |
| Country Road South of Oxley Highway | 0 | 4 | 4 |
| Duri Road <br> South of Gunnedah Road | 560 | 164 | 724 |
| Bridge Street <br> North of Gunnedah Road | 560 | 116 | 676 |
| Wallamore Road West of Goddard Lane | 40 | 0 | 40 |
| Wallamore Road East of Goddard Lane | 748 | 0 | 748 |
| Jewry Street <br> North of Wallamore Road | 748 | 0 | 748 |

A trip is a one way movement, a vehicle arriving then departing generates two vehicle trips on the road network

### 3.6 Construction Traffic Generation and Distribution

Details of the construction programming and vehicle requirements are not yet known. It is however expected that construction activity is likely to occur during daytime hours, six days per week, and that the initial construction activity would involve construction of the new vehicle access. This would be followed by construction of the processing plant infrastructure within the site.

Construction activity would generate vehicle trips on the surrounding road network due to the construction workforce travelling to and from the site each day, and due to deliveries of materials and equipment. Peak vehicle trips each day would typically occur at the start of
transport planning
the day when the majority of the construction workforce arrive on site, and at the end of the day when the workforce leave the site. Assuming that the typical work hours would be between 7:00 am and 6:00 pm, the morning peak would occur before 7:00 am, and the evening peak would occur after 6:00 pm. Heavy vehicle deliveries would be spread throughout the day, and would not tend to coincide with the peak movement of the workforce to and from the site.

The construction workforce would be significantly fewer people than the forecast operational workforce at the processing plant, and the number of heavy vehicle deliveries during construction would be significantly lower than the heavy vehicle trips expected to be generated by the processing plant when operational. The number of light and heavy vehicle trips generated by the construction activity is therefore anticipated to be significantly lower than that of the operational processing plant as presented in Section 3.4. The peak times for vehicle trip generation during construction would be earlier than the on-street morning peak hour and later than the on-street afternoon peak hour (Table 2.3).

Construction vehicles accessing the site for the initial construction of the new access would travel directly to and from the new access location via Armstrong Street and Goddard Lane and would not use the existing access from Oxley Highway. Once the new access is commissioned, all vehicles generated by the construction activity for the processing plant would access the site via the new access. Adequate space would be available on-site to park all construction workforce and delivery vehicles, so construction traffic would not impact on local on-street parking conditions.

Considering that the number of trips generated during the construction stage would be significantly lower than during the operational stage, and that construction vehicles would use the same access routes as the operational traffic, separate assessment of the impacts of construction traffic on the operation of the road network is not warranted. The traffic impacts of the construction stage will be less than that of the operational stage, which are assessed in Section 5.
transport planning

## 4 Future Baseline Traffic Conditions

This section assesses the future traffic conditions without the proposed processing plant, to form a baseline against which the impacts of the processing plant can be assessed. These future conditions are described in this section.

### 4.1 Background Traffic Growth

It is generally expected that growth in traffic will occur on the road network over time. Such growth may be related to the impacts of a particular development or to non-specific growth as population changes and people's travel behaviour changes. For the purpose of this assessment, a background growth rate of 2.0 percent per year is assumed to occur on all the public roads serving the site.

### 4.2 Future Baseline Traffic Volumes

Table 4.1 summarises the peak hourly and daily traffic volumes expected to occur with continuation of the existing rendering plant, and with an indicative 10 years of growth in background traffic (i.e. traffic not associated with the site) as described above.

Table 4.1: Future Weekday Traffic Volumes with Background Growth

| Road and Location | AM Peak Hour |  | PM Peak Hour |  | Vehicles per Day | Percent Heavy (\%) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Hour Start | Vehicles per Hour | Hour Start | Vehicles per Hour |  |  |
| Oxley Highway <br> North of Joshua Street | 8:00 | 311 | 16:00 | 369 | 3,955 | 18.8 |
| Oxley Highway <br> South of Byamee Lane | 8:00 | 350 | 16:00 | 385 | 4,367 | 19.9 |
| Oxley Highway <br> North of Baiada Access | 8:00 | 364 | 15:00 | 409 | 4,753 | 18.3 |
| Oxley Highway <br> North of Goddard Lane | 8:00 | 424 | 15:00 | 472 | 5,339 | 17.5 |
| Oxley Highway South of Goddard Lane | 8:00 | 365 | 15:00 | 578 | 6,030 | 17.1 |
| Oxley Highway East of Evans Street | 9:00 | 778 | 15:00 | 1,025 | 10,204 | 10.6 |
| Oxley Highway East of Edith Street | 8:00 | 1,210 | 15:00 | 1,449 | 16,154 | 14.5 |
| Wallamore Road South of Goddard Lane | 8:00 | 324 | 15:00 | 526 | 4,839 | 16.0 |
| Manilla Road South of Browns Lane | 8:00 | 468 | 16:00 | 480 | 5,331 | 9.3 |
| New England Highway South of Hall Street | 8:00 | 1,268 | 16:00 | 1,317 | 14,525 | 9.8 |
| Duri Road South of Bylong Road | 8:00 | 439 | 16:00 | 429 | 4,918 | 17.7 |
| Goonoo Goonoo Road North of Burgmanns Lane | 8:00 | 657 | 17:00 | 684 | 8,147 | 15.3 |
| Appleby Lane <br> East of Oxley Highway | 7:00 | 58 | 16:00 | 61 | 641 | 21.2 |
| Bridge Street at Peel River Bridge | 8:00 | 2,414 | 15:00 | 2,736 | 30,820 | 7.9 |
| Jewry Street <br> West of Wirraway Street | 8:00 | 1,211 | 15:00 | 1,294 | 14,361 | 15.7 |

Assumes growth of non-site generated traffic at 2 percent per annum from survey year to 2028

### 4.3 Future Baseline Road Network Performance

Table 4.2 summarises the resulting peak hour midblock levels of service expected with continuance of the existing rendering plant and an increase in background traffic at 2 percent per year over 10 years. The background traffic is the surveyed traffic not generated by the existing rendering plant. As noted previously, while the location south of Goddard Lane has been assessed for its midblock performance, the operation of the intersections in the vicinity are expected to be the primary determinant of network performance. The intersection performance is discussed in Section 4.4.

Table 4.2: Future Weekday Peak Hour Midblock Performance with Background Growth

| Road and Location | Class | Inbound to <br> Processing Plant |  | Outbound from <br> Processing Plant |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | PTSF | LOS | PTSF | LOS |
| AM Peak Hour |  |  |  |  |  |
| PM Peak Hour | ॥ | 45.1 | B | 32.8 | A |
| Oxley Highway <br> South of Goddard Lane |  | 45.7 | B | 43.8 | B |
| AM Peak Hour |  |  |  |  |  |
| PM Peak Hour | $\\|$ | 26.5 | A | 26.7 | A |

The results indicate that the level of service experienced by drivers on Oxley Highway near the site would remain satisfactory if the rendering plant were to continue operating with background traffic growth.

### 4.4 Future Baseline Intersection Operation

Table 5.3 summarises the resulting peak hour operating conditions with the assumed coincidence of peak activity as above, and an increase in background traffic at 2 percent per year over 10 years. The background traffic is the surveyed traffic not generated by the existing rendering plant.

Table 4.3: Peak Hour Intersection Operation with Background Growth

| Intersection | AM Peak Hour |  |  | PM Peak Hour |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
|  | X-Value | Average <br> Delay | Level of <br> Service | X-Value | Average <br> Delay | Level of <br> Service |
| Oxley Highway and <br> Goddard Lane | 0.17 | 11.9 | A | 0.32 | 13.5 | A |
| Goddard Lane and <br> Armstrong Street | 0.09 | 8.2 | A | 0.13 | 8.7 | A |
| Goddard Lane and <br> Wallamore Road | 0.18 | 8.7 | A | 0.35 | A | A |
| Oxley Highway and <br> Duri Road | 0.45 | 12.2 | A | 0.39 | A |  |
| Oxley Highway and <br> Marius Street | 0.86 | 32.4 | C | 0.87 | C |  |
| Peel Street and <br> Jewry Street | $>1.0$ | 54.6 | D | $>1.0$ | A | F |

These results assume that the existing signal timing would remain unchanged at the intersection of Oxley Highway with Marius Street from that observed during the surveys in 2018. The results demonstrate that the intersections are forecast to operate with satisfactory levels of service and spare capacity, with the exception of the roundabout at Peel Street and Jewry Street, at which demand is forecast to exceed capacity with the increase in
transport planning
background traffic. As noted previously, adjustments to line marking at the roundabout would provide for additional capacity by allowing drivers to safely turn left from Jewry Street to Peel Street and from Peel Street to Jewry Street unopposed by circulating or exiting traffic. The results of the analysis suggest that this additional capacity will be required in the future even without the proposed processing plant.

## 5 Impacts of the Processing Plant

### 5.1 Future Traffic Volumes

Table 5.1 summarises the peak hourly and daily traffic volumes expected to occur with the processing plant at surveyed locations on the road network. These represent conditions if the processing plant were operating with an indicative 10 years of growth in background traffic (i.e. traffic not associated with the site).

Table 5.1: Weekday Traffic Volumes with Background Growth and Processing Plant

| Road and Location | AM Peak Hour |  | PM Peak Hour |  | Vehicles per Day | Percent Heavy (\%) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Hour Start | Vehicles per Hour | Hour Start | Vehicles per Hour |  |  |
| Oxley Highway <br> North of Joshua Street | 8:00 | 314 | 16:00 | 373 | 4,063 | 19.6 |
| Oxley Highway South of Byamee Lane | 8:00 | 357 | 16:00 | 393 | 4,537 | 21.6 |
| Oxley Highway <br> North of Baiada Access | 8:00 | 371 | 15:00 | 420 | 4,963 | 19.8 |
| Oxley Highway <br> North of Goddard Lane | 8:00 | 429 | 15:00 | 478 | 5,545 | 18.4 |
| Oxley Highway <br> South of Goddard Lane | 8:00 | 374 | 15:00 | 698 | 7,346 | 17.1 |
| Oxley Highway East of Evans Street | 9:00 | 796 | 15:00 | 1,146 | 11,524 | 11.3 |
| Oxley Highway <br> East of Edith Street | 8:00 | 1,220 | 15:00 | 1,570 | 17,474 | 14.7 |
| Wallamore Road South of Goddard Lane | 8:00 | 324 | 15:00 | 601 | 5,587 | 13.8 |
| Manilla Road South of Browns Lane | 8:00 | 472 | 16:00 | 484 | 5,397 | 10.4 |
| New England Highway South of Hall Street | 8:00 | 1,272 | 16:00 | 1,323 | 14,690 | 10.5 |
| Duri Road South of Bylong Road | 8:00 | 447 | 16:00 | 438 | 5,117 | 19.9 |
| Goonoo Goonoo Road North of Burgmanns Lane | 8:00 | 665 | 17:00 | 690 | 8,346 | 16.6 |
| Appleby Lane East of Oxley Highway | 7:00 | 61 | 16:00 | 65 | 703 | 28.1 |
| Bridge Street at Peel River Bridge | 8:00 | 2,418 | 15:00 | 2,778 | 31,312 | 8.1 |
| Jewry Street West of Wirraway Street | 8:00 | 1,211 | 15:00 | 1,368 | 15,103 | 14.9 |

Assumes growth of non-site generated traffic at 2 percent per annum from survey year to 2018 and 2028

### 5.2 Future Road Network Performance

Table 5.2 summarises the resulting peak hour midblock levels of service expected with the proposed processing plant operating, together with an increase in background traffic at 2 percent per year over 10 years. As noted previously, while the location south of Goddard Lane has been assessed for its midblock performance, the operation of the intersections in the vicinity are expected to be the primary determinant of network performance. The forecast intersection performance with the processing plant is discussed in Section 5.3.

Table 5.2: Weekday Peak Hour Midblock Performance with Growth and Processing Plant

| Road and Location | Class | Inbound to Processing Plant |  | Outbound from Processing Plant |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | PTSF | LOS | PTSF | LOS |
| Oxley Highway <br> North of Existing Site Access |  |  |  |  |  |
| AM Peak Hour | 11 | 49.4 | B | 37.5 | A |
| PM Peak Hour | II | 48.2 | B | 50.8 | B |
| Oxley Highway <br> South of Goddard Lane |  |  |  |  |  |
| AM Peak Hour | II | 31.6 | A | 32.0 | A |
| PM Peak Hour | II | 40.1 | B | 56.1 | C |

The results demonstrate that the midblock level of service experienced by drivers is expected to remain satisfactory with the combined effects of background traffic growth and the processing plant traffic.

### 5.3 Future Intersection Operation

The impact of the processing plant traffic on the operation of intersections has been assessed using SIDRA INTERSECTION. As noted (Section 3.4.3) the expected traffic generation of the processing plant is low during the on-street peak hours, with site-generated peaks occurring outside of the on-street peaks. The processing plant traffic would therefore make only a minor contribution to the on-street peak hour operating conditions of the key intersections, noting that intersections are typically the critical locations with respect to the capacity of the road network, due to the need for conflicting vehicles to occupy the same road space.

As a robust assessment of the future operating conditions, the analysis has assumed that the peak volume of additional traffic resulting from the processing plant during the surveyed morning and afternoon periods ( 6 am to 9 am and 3 pm to 7 pm ) would coincide with the surveyed peak volumes over those same periods. This will result in an overestimate of the future peak hour conditions, as those peaks are unlikely to coincide.

Table 5.3 summarises the resulting peak hour operating conditions with the assumed coincidence of peak activity as above based on surveyed traffic conditions in 2018. These
transport planning
results assume that the existing signal timing would remain unchanged at the intersection of Oxley Highway with Marius Street from that observed during the surveys in 2018.

Table 5.3: Peak Hour Intersection Operation with Processing Plant (2018)

| Intersection | AM Peak Hour |  |  | PM Peak Hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | X-Value | Average Delay | Level of Service | X-Value | Average Delay | Level of Service |
| Oxley Highway and Goddard Lane | 0.16 | 11.9 | A | 0.38 | 13.1 | A |
| Goddard Lane and Armstrong Street | 0.11 | 7.7 | A | 0.30 | 8.5 | A |
| Goddard Lane and Wallamore Road | 0.15 | 8.6 | A | 0.37 | 9.5 | A |
| Oxley Highway and Duri Road | 0.36 | 11.6 | A | 0.33 | 10.5 | A |
| Oxley Highway and Marius Street | 0.69 | 29.4 | C | 0.77 | 33.0 | C |
| Peel Street and Jewry Street | 0.77 | 16.9 | B | 0.89 | 19.6 | B |

The SIDRA results demonstrate that with the traffic changes forecast to result from the processing plant, the key intersections would continue to operate at good levels of service. As noted, the forecasts assume a "worst case" in which the peak traffic generated by the processing plant would coincide with the on-street peak conditions, which is unlikely to occur. Nevertheless, the results indicate that sufficient capacity is available at the intersections under such conditions.

Table 5.4 summarises the longer term peak hour operating conditions with the assumed coincidence of peak activity as above, and an increase in background traffic at 2 percent per year over 10 years. As above, these results assume that the existing signal timing would remain unchanged at the intersection of Oxley Highway with Marius Street from that observed during the surveys in 2018.

Table 5.4: Peak Hour Intersection Operation with Processing Plant and Growth to 2028

| Intersection | AM Peak Hour |  |  | PM Peak Hour |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
|  | X-Value | Average <br> Delay | Level of <br> Service | X-Value | Average <br> Delay | Level of <br> Service |
| Oxley Highway and <br> Goddard Lane | 0.20 | 13.2 | A | 0.47 | 15.9 | B |
| Goddard Lane and <br> Armstrong Street | 0.13 | 7.9 | A | 0.34 | 8.8 | A |
| Goddard Lane and <br> Wallamore Road | 0.19 | 8.8 | A | 0.45 | 10.0 | A |
| Oxley Highway and <br> Duri Road | 0.46 | 12.3 | A | 0.41 | 10.9 | A |
| Oxley Highway and <br> Marius Street | 0.86 | 32.4 | C | 0.92 | C |  |
| Peel Street and <br> Jewry Street | $>1.0$ | 57.3 | E | $>1.0$ | F |  |

The results demonstrate that with the combined effects of background traffic growth and the processing plant traffic, the intersections are forecast to operate with satisfactory levels of service and spare capacity. As discussed in Section 4.4, the exception is the roundabout at Peel Street and Jewry Street, at which the baseline traffic demand is forecast to exceed capacity with the increase in background traffic. As noted, adjustments to line marking at the roundabout would provide for additional capacity by allowing drivers to safely turn left from Jewry Street to Peel Street and from Peel Street to Jewry Street unopposed by circulating or exiting traffic. The results of the analysis suggest that this additional capacity will be required in the future without the proposed processing plant.

### 5.4 Road Safety Implications

The review of the road safety history of the key access routes has not highlighted any particular causal factors which may be exacerbated by the processing plant traffic. The intersections of Oxley Highway with Goddard Lane, and Wallamore Road with Goddard Lane have been recently upgraded and are suitably designed for use by the heavy vehicles associated with the existing industrial area and the proposed processing plant. The forecast operating conditions at the intersections would not result in excess delays to vehicles that may encourage drivers to take unnecessary risks.

### 5.5 Car Parking Provision

Tamworth Regional Development Control Plan 2010 requires that car parking at light or heavy industry developments be provided at the greater of one space per $75 \mathrm{~m}^{2}$ GFA or one space per two employees. On this basis, the processing plant requires a minimum of 632 spaces based on the proposed $47,348 \mathrm{~m}^{2}$ GFA or 588 spaces based on the total of 1,176 employees. The proposed provision of 820 car parking spaces therefore exceeds the requirements of the DCP and is satisfactory.

By way of comparison, on the basis of the expected staff attendance pattern (refer to Section 3.4.2) and average car occupancy, the demand for staff car parking throughout the day has been estimated, as shown in Figure 5.1.

Figure 5.1: Processing Plant Staff Parking Demand


The peak demand for staff car parking would occur in the early afternoon, at 698 spaces, based on the travel patterns of staff described in Section 3.4.2. The proposed provision of 820 car parking spaces on the site would therefore accommodate the expected peak parking demand within the site, and is satisfactory.

The DCP does not specify a particular rate for the provision of car parking spaces for people with a disability. The proposed provision of eight spaces is equivalent to one per cent of the total number of spaces, which is consistent with the Building Code of Australia's requirement and is therefore considered satisfactory.

### 5.6 Access and Internal Layout

The design of the staff car parking area has been reviewed with regard to Australian Standard 2890.1 (2004). The design meets or exceeds the minimum requirements of that Standard with regard to the dimensions of the parking bays, aisles and driveway access road. "Type 1" speed humps are provided in the long aisles and driveway in accordance with AS2890.1 to provide positive speed control.

The spaces allocated to people with a disability are proposed to be designed and marked in accordance with the Australian Standard AS2890.6 (2009).

The internal layout of the processing plant roadways has been assessed for suitability by considering the swept paths of the heavy vehicles expected to use the site. The proposed road layouts are satisfactory for manoeuvring of those vehicles, and will allow for fire truck access through the car park from Oxley Highway if required.

It is noted that the internal roundabout at the entry to the staff car park is not required on capacity grounds, as the approaches of the existing site driveway would be used only infrequently for emergency access. The intersection may instead be appropriately constructed as a simple cross intersection, with priority being along the road into and out of the staff car park. If constructed, the central island of the roundabout would be required to be fully mountable to ensure emergency vehicle access (including fire trucks) remains available.

The proposed layout of internal roads has been assessed for use by B-doubles, and is satisfactory.

### 5.7 Mitigation Measures

This assessment has found that the traffic generated by the processing plant can generally be accommodated by the existing road network, without requiring any specific measures to address safety or capacity concerns.

The exception to this is the roundabout at the intersection of Peel Street and Jewry Street, which is expected to reach capacity with future traffic growth, regardless of traffic generated by the processing plant. As discussed, minor amendments to linemarking of the roundabout would provide additional capacity by proving better guidance and lane discipline for the circulating and exiting traffic. Such amendments would permit vehicles to turn left from Jewry Street to Peel Street without needing to give way to circulating traffic in the inner lane of the roundabout, being predominantly the westbound through vehicles on Peel Street. Improved lane marking would require those westbound vehicles to remain in the right hand lane when exiting the roundabout. The left turning vehicles from Jewry Street would turn into the left hand lane when exiting the roundabout.

Similarly amendments to the linemarking would permit vehicles to turn left from Peel Street to Jewry Street without needing to give way to circulating traffic in the inner lane of the roundabout, being predominantly those vehicles turning right from Peel Street to Jewry Street. Improved lane marking would require those right turning vehicles to remain in the right hand lane when exiting the roundabout, while the left turning vehicles from Peel Street would turn into the left hand lane when exiting the roundabout.
transport planning

These amendments are not the result of the processing plant, rather will provide additional capacity at the roundabout to meet the forecast increase in demand resulting from general background traffic growth in the region.
transport planning

## 6 Conclusions

This assessment of the road transport implications of a proposed processing plant on the site of the Oakburn rendering plant near Tamworth has found that the existing road network has sufficient capacity to accommodate the traffic generated by the processing plant with acceptable impacts on the operation of the key intersections.

The proposed provision of staff car parking is expected to meet the requirements of the processing plant staff and visitors.

The proposed layout of the staff car park complies with the relevant Australian Standards. The layout of the internal road network and car parking is satisfactory for the vehicles expected to use it.

The roundabout at Peel Street and Jewry Street is expected to reach capacity with background growth in traffic which is unrelated to the proposed processing plant. Additional capacity may be gained by improvements to the linemarking of the roundabout.

## Appendix A

## Traffic Surveys

| Job No | Q2118 - Tamworth |  |
| :--- | :--- | :--- |
| Client | TTPP |  |
| Site | Oxley Highway (North of Baiada Site Access) |  |
| Location | Tamworth |  |
| Site No | 1 |  |
| Start Date | $27-J u n-18$ |  |
| Description | Volume Summary |  |
| Direction | Combined |  |


| Hour <br> Starting | Day of Week |  |  |  |  |  |  | W'Day Ave 3963 | 7 Day Ave 3704 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Mon | Tue | Wed | Thu | Fri | Sat | Sun |  |  |
|  | 2-Jul | 3-Jul | 27-Jun | 28-Jun | 29-Jun | 30-Jun | 1-Jul |  |  |
| AM Peak | 284 | 292 | 322 | 333 | 303 | 327 | 243 |  |  |
| PM Peak | 296 | 336 | 351 | 376 | 402 | 279 | 289 |  |  |
| 0:00 | 6 | 12 | 11 | 9 | 10 | 13 | 26 | 10 | 12 |
| 1:00 | 2 | 5 | 9 | 7 | 4 | 8 | 5 | 5 | 6 |
| 2:00 | 8 | 4 | 4 | 4 | 4 | 4 | 9 | 5 | 5 |
| 3:00 | 13 | 19 | 15 | 14 | 28 | 12 | 9 | 18 | 16 |
| 4:00 | 42 | 45 | 37 | 34 | 44 | 26 | 10 | 40 | 34 |
| 5:00 | 84 | 94 | 75 | 77 | 92 | 41 | 22 | 84 | 69 |
| 6:00 | 164 | 171 | 162 | 163 | 178 | 77 | 43 | 168 | 137 |
| 7:00 | 260 | 247 | 256 | 241 | 226 | 102 | 73 | 246 | 201 |
| 8:00 | 269 | 292 | 322 | 333 | 303 | 214 | 131 | 304 | 266 |
| 9:00 | 284 | 229 | 275 | 294 | 299 | 299 | 198 | 276 | 268 |
| 10:00 | 282 | 249 | 250 | 276 | 271 | 285 | 196 | 266 | 258 |
| 11:00 | 260 | 230 | 258 | 285 | 274 | 327 | 243 | 261 | 268 |
| 12:00 | 250 | 266 | 254 | 248 | 312 | 275 | 259 | 266 | 266 |
| 13:00 | 262 | 249 | 257 | 313 | 336 | 279 | 247 | 283 | 278 |
| 14:00 | 296 | 288 | 319 | 349 | 366 | 274 | 289 | 324 | 312 |
| 15:00 | 281 | 281 | 351 | 376 | 402 | 268 | 263 | 338 | 317 |
| 16:00 | 286 | 336 | 345 | 359 | 377 | 254 | 251 | 341 | 315 |
| 17:00 | 273 | 297 | 290 | 290 | 308 | 226 | 176 | 292 | 266 |
| 18:00 | 172 | 159 | 145 | 197 | 211 | 143 | 105 | 177 | 162 |
| 19:00 | 77 | 78 | 74 | 100 | 97 | 69 | 61 | 85 | 79 |
| 20:00 | 66 | 63 | 50 | 90 | 73 | 55 | 45 | 68 | 63 |
| 21:00 | 47 | 46 | 37 | 56 | 56 | 44 | 41 | 48 | 47 |
| 22:00 | 33 | 35 | 40 | 32 | 55 | 54 | 16 | 39 | 38 |
| 23:00 | 12 | 14 | 19 | 19 | 29 | 38 | 7 | 19 | 20 |
| Total | 3729 | 3709 | 3855 | 4166 | 4355 | 3387 | 2725 | 3963 | 3704 |


| $7-19$ | 3175 | 3123 | 3322 | 3561 | 3685 | 2946 | 2431 | 3373 | 3178 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $6-22$ | 3529 | 3481 | 3645 | 3970 | 4089 | 3191 | 2621 | 3743 | 3504 |
| $6-24$ | 3574 | 3530 | 3704 | 4021 | 4173 | 3283 | 2644 | 3800 | 3561 |
| $0-24$ | 3729 | 3709 | 3855 | 4166 | 4355 | 3387 | 2725 | 3963 | 3704 |


| Job No | Q2118 - Tamworth |  |
| :--- | :--- | :--- |
| Client | TTPP |  |
| Site | Oxley Highway (South of Goddard Lane) |  |
| Location | Tamworth |  |
| Site No | 2 |  |
| Start Date | 27-Jun-18 |  |
| Description | Volume Summary |  |
| Direction | Combined |  |


| Hour <br> Starting | Day of Week |  |  |  |  |  |  | W'Day <br> Ave <br> 5040 | 7 Day <br> Ave <br> 4512 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Mon | Tue | Wed | Thu | Fri | Sat | Sun |  |  |
|  | 2-Jul | 3-Jul | 27-Jun | 28-Jun | 29-Jun | 30-Jun | 1-Jul |  |  |
| AM Peak | 319 | 304 | 306 | 306 | 325 | 313 | 245 |  |  |
| PM Peak | 452 | 474 | 485 | 525 | 616 | 310 | 269 |  |  |
| 0:00 | 16 | 36 | 47 | 74 | 44 | 35 | 25 | 43 | 40 |
| 1:00 | 8 | 49 | 66 | 46 | 61 | 43 | 11 | 46 | 41 |
| 2:00 | 20 | 61 | 50 | 68 | 52 | 65 | 13 | 50 | 47 |
| 3:00 | 56 | 60 | 62 | 60 | 77 | 32 | 7 | 63 | 51 |
| 4:00 | 168 | 176 | 164 | 153 | 171 | 45 | 12 | 166 | 127 |
| 5:00 | 182 | 218 | 195 | 205 | 214 | 154 | 27 | 203 | 171 |
| 6:00 | 245 | 247 | 239 | 232 | 252 | 108 | 52 | 243 | 196 |
| 7:00 | 317 | 275 | 302 | 265 | 264 | 137 | 70 | 285 | 233 |
| 8:00 | 282 | 304 | 306 | 306 | 325 | 205 | 135 | 305 | 266 |
| 9:00 | 311 | 258 | 278 | 271 | 314 | 249 | 189 | 286 | 267 |
| 10:00 | 306 | 252 | 231 | 275 | 306 | 252 | 176 | 274 | 257 |
| 11:00 | 319 | 232 | 252 | 267 | 308 | 313 | 245 | 276 | 277 |
| 12:00 | 291 | 275 | 260 | 296 | 395 | 299 | 254 | 303 | 296 |
| 13:00 | 306 | 310 | 294 | 361 | 390 | 267 | 239 | 332 | 310 |
| 14:00 | 376 | 364 | 367 | 426 | 488 | 248 | 269 | 404 | 363 |
| 15:00 | 384 | 405 | 485 | 525 | 616 | 260 | 250 | 483 | 418 |
| 16:00 | 452 | 474 | 437 | 517 | 490 | 252 | 245 | 474 | 410 |
| 17:00 | 289 | 293 | 307 | 289 | 309 | 310 | 188 | 297 | 284 |
| 18:00 | 170 | 169 | 138 | 177 | 210 | 145 | 110 | 173 | 160 |
| 19:00 | 97 | 86 | 91 | 101 | 108 | 58 | 71 | 97 | 87 |
| 20:00 | 64 | 72 | 61 | 97 | 94 | 52 | 54 | 78 | 71 |
| 21:00 | 52 | 57 | 41 | 66 | 65 | 43 | 38 | 56 | 52 |
| 22:00 | 46 | 50 | 44 | 36 | 65 | 59 | 20 | 48 | 46 |
| 23:00 | 54 | 62 | 30 | 55 | 69 | 43 | 9 | 54 | 46 |
| Total | 4811 | 4785 | 4747 | 5168 | 5687 | 3674 | 2709 | 5040 | 4512 |


| $7-19$ | 3803 | 3611 | 3657 | 3975 | 4415 | 2937 | 2370 | 3892 | 3538 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $6-22$ | 4261 | 4073 | 4089 | 4471 | 4934 | 3198 | 2585 | 4366 | 3944 |
| $6-24$ | 4361 | 4185 | 4163 | 4562 | 5068 | 3300 | 2614 | 4468 | 4036 |
| $0-24$ | 4811 | 4785 | 4747 | 5168 | 5687 | 3674 | 2709 | 5040 | 4512 |


| Job No | Q2118 - Tamworth |  |
| :--- | :--- | :--- |
| Client | TTPP |  |
| Site | Wallamore Rd (South of Goddard Lane) |  |
| Location | Tamworth |  |
| Site No | 3 |  |
| Start Date | 27-Jun-18 |  |
| Description | Volume Summary |  |
| Direction | Combined |  |
|  |  |  |


| Hour Starting | Day of Week |  |  |  |  |  |  | W'Day Ave 4033 | 7 Day Ave 3385 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Mon | Tue | Wed | Thu | Fri | Sat | Sun |  |  |
|  | 2-Jul | 3-Jul | 27-Jun | 28-Jun | 29-Jun | 30-Jun | 1-Jul |  |  |
| AM Peak | 267 | 259 | 283 | 283 | 271 | 216 | 154 |  |  |
| PM Peak | 400 | 409 | 440 | 441 | 501 | 171 | 137 |  |  |
| 0:00 | 7 | 26 | 51 | 58 | 29 | 19 | 6 | 34 | 28 |
| 1:00 | 5 | 43 | 52 | 40 | 50 | 30 | 3 | 38 | 32 |
| 2:00 | 15 | 72 | 58 | 72 | 60 | 74 | 3 | 55 | 51 |
| 3:00 | 29 | 39 | 40 | 27 | 38 | 19 | 8 | 35 | 29 |
| 4:00 | 139 | 138 | 124 | 130 | 142 | 24 | 4 | 135 | 100 |
| 5:00 | 137 | 141 | 158 | 164 | 142 | 125 | 11 | 148 | 125 |
| 6:00 | 200 | 203 | 171 | 179 | 175 | 93 | 29 | 186 | 150 |
| 7:00 | 226 | 209 | 222 | 212 | 205 | 64 | 47 | 215 | 169 |
| 8:00 | 253 | 259 | 283 | 283 | 270 | 103 | 48 | 270 | 214 |
| 9:00 | 263 | 191 | 241 | 258 | 248 | 177 | 86 | 240 | 209 |
| 10:00 | 259 | 204 | 197 | 224 | 263 | 216 | 102 | 229 | 209 |
| 11:00 | 267 | 205 | 235 | 232 | 271 | 196 | 154 | 242 | 223 |
| 12:00 | 275 | 216 | 236 | 204 | 295 | 171 | 137 | 245 | 219 |
| 13:00 | 254 | 237 | 252 | 272 | 343 | 137 | 109 | 272 | 229 |
| 14:00 | 364 | 334 | 355 | 371 | 359 | 148 | 133 | 357 | 295 |
| 15:00 | 400 | 409 | 440 | 441 | 501 | 128 | 113 | 438 | 347 |
| 16:00 | 382 | 393 | 394 | 383 | 372 | 130 | 117 | 385 | 310 |
| 17:00 | 208 | 244 | 227 | 216 | 226 | 156 | 97 | 224 | 196 |
| 18:00 | 118 | 76 | 91 | 101 | 101 | 63 | 62 | 97 | 87 |
| 19:00 | 39 | 52 | 48 | 55 | 46 | 31 | 29 | 48 | 43 |
| 20:00 | 47 | 30 | 19 | 40 | 39 | 20 | 17 | 35 | 30 |
| 21:00 | 44 | 27 | 44 | 32 | 30 | 19 | 15 | 35 | 30 |
| 22:00 | 23 | 13 | 17 | 19 | 24 | 20 | 10 | 19 | 18 |
| 23:00 | 65 | 64 | 24 | 51 | 48 | 15 | 11 | 50 | 40 |
| Total | 4019 | 3825 | 3979 | 4064 | 4277 | 2178 | 1351 | 4033 | 3385 |


| $7-19$ | 3269 | 2977 | 3173 | 3197 | 3454 | 1689 | 1205 | 3214 | 2709 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $6-22$ | 3599 | 3289 | 3455 | 3503 | 3744 | 1852 | 1295 | 3518 | 2962 |
| $6-24$ | 3687 | 3366 | 3496 | 3573 | 3816 | 1887 | 1316 | 3588 | 3020 |
| $0-24$ | 4019 | 3825 | 3979 | 4064 | 4277 | 2178 | 1351 | 4033 | 3385 |


| Job No | Q2118 - Tamworth |  |
| :--- | :--- | :--- |
| Client | TTPP |  |
| Site | Manilla Rd (South of Browns Lane) |  |
| Location | Tamworth |  |
| Site No | 4 |  |
| Start Date | 27-Jun-18 |  |
| Description | Volume Summary |  |
| Direction | Combined |  |
|  |  |  |


| Hour <br> Starting | Day of Week |  |  |  |  |  |  | W'Day Ave 4443 | 7 Day <br> Ave <br> 4152 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Mon | Tue | Wed | Thu | Fri | Sat | Sun |  |  |
|  | 2-Jul | 3-Jul | 27-Jun | 28-Jun | 29-Jun | 30-Jun | 1-Jul |  |  |
| AM Peak | 347 | 374 | 403 | 435 | 393 | 371 | 273 |  |  |
| PM Peak | 363 | 384 | 397 | 414 | 443 | 340 | 280 |  |  |
| 0:00 | 6 | 13 | 11 | 10 | 9 | 12 | 27 | 10 | 13 |
| 1:00 | 7 | 8 | 4 | 6 | 7 | 8 | 17 | 6 | 8 |
| 2:00 | 4 | 11 | 9 | 4 | 7 | 10 | 12 | 7 | 8 |
| 3:00 | 11 | 13 | 19 | 13 | 16 | 12 | 3 | 14 | 12 |
| 4:00 | 40 | 47 | 40 | 42 | 54 | 23 | 15 | 45 | 37 |
| 5:00 | 93 | 80 | 96 | 80 | 78 | 39 | 25 | 85 | 70 |
| 6:00 | 178 | 170 | 177 | 178 | 157 | 73 | 40 | 172 | 139 |
| 7:00 | 288 | 298 | 305 | 277 | 262 | 144 | 81 | 286 | 236 |
| 8:00 | 347 | 374 | 403 | 435 | 393 | 291 | 108 | 390 | 336 |
| 9:00 | 335 | 341 | 343 | 361 | 352 | 322 | 188 | 346 | 320 |
| 10:00 | 279 | 249 | 292 | 293 | 297 | 371 | 239 | 282 | 289 |
| 11:00 | 259 | 253 | 285 | 255 | 329 | 338 | 273 | 276 | 285 |
| 12:00 | 232 | 234 | 258 | 257 | 302 | 340 | 274 | 257 | 271 |
| 13:00 | 277 | 288 | 284 | 275 | 334 | 313 | 243 | 292 | 288 |
| 14:00 | 278 | 288 | 316 | 335 | 352 | 279 | 258 | 314 | 301 |
| 15:00 | 356 | 352 | 330 | 372 | 422 | 284 | 280 | 366 | 342 |
| 16:00 | 363 | 383 | 397 | 414 | 443 | 269 | 219 | 400 | 355 |
| 17:00 | 356 | 384 | 361 | 372 | 423 | 292 | 212 | 379 | 343 |
| 18:00 | 177 | 202 | 224 | 217 | 228 | 197 | 137 | 210 | 197 |
| 19:00 | 103 | 113 | 113 | 120 | 117 | 102 | 72 | 113 | 106 |
| 20:00 | 81 | 77 | 85 | 83 | 82 | 67 | 69 | 82 | 78 |
| 21:00 | 48 | 49 | 55 | 58 | 77 | 82 | 43 | 57 | 59 |
| 22:00 | 29 | 32 | 26 | 28 | 61 | 62 | 23 | 35 | 37 |
| 23:00 | 16 | 15 | 12 | 16 | 30 | 43 | 17 | 18 | 21 |
| Total | 4163 | 4274 | 4445 | 4501 | 4832 | 3973 | 2875 | 4443 | 4152 |


| $7-19$ | 3547 | 3646 | 3798 | 3863 | 4137 | 3440 | 2512 | 3798 | 3563 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $6-22$ | 3957 | 4055 | 4228 | 4302 | 4570 | 3764 | 2736 | 4222 | 3945 |
| $6-24$ | 4002 | 4102 | 4266 | 4346 | 4661 | 3869 | 2776 | 4275 | 4003 |
| $0-24$ | 4163 | 4274 | 4445 | 4501 | 4832 | 3973 | 2875 | 4443 | 4152 |


| Job No | Q2118 - Tamworth |  |
| :--- | :--- | :--- |
| Client | TTPP |  |
| Site | New England Highway (South of Hall St) |  |
| Location | Tamworth |  |
| Site No | 5 |  |
| Start Date | 27-Jun-18 |  |
| Description | Volume Summary |  |
| Direction | Combined |  |
|  |  |  |


| Hour <br> Starting | Day of Week |  |  |  |  |  |  | W'Day Ave 12106 | 7 Day <br> Ave <br> 11151 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Mon | Tue | Wed | Thu | Fri | Sat | Sun |  |  |
|  | 2-Jul | 3-Jul | 27-Jun | 28-Jun | 29-Jun | 30-Jun | 1-Jul |  |  |
| AM Peak | 1116 | 1003 | 1022 | 1068 | 1074 | 952 | 792 |  |  |
| PM Peak | 1079 | 1063 | 1104 | 1163 | 1145 | 830 | 787 |  |  |
| 0:00 | 20 | 39 | 32 | 46 | 54 | 39 | 60 | 38 | 41 |
| 1:00 | 20 | 40 | 25 | 20 | 44 | 51 | 25 | 30 | 32 |
| 2:00 | 15 | 22 | 21 | 29 | 25 | 27 | 24 | 22 | 23 |
| 3:00 | 23 | 38 | 39 | 40 | 29 | 30 | 14 | 34 | 30 |
| 4:00 | 72 | 70 | 70 | 73 | 80 | 48 | 26 | 73 | 63 |
| 5:00 | 182 | 183 | 185 | 190 | 193 | 112 | 55 | 187 | 157 |
| 6:00 | 375 | 367 | 436 | 399 | 409 | 133 | 130 | 397 | 321 |
| 7:00 | 725 | 637 | 659 | 665 | 690 | 296 | 221 | 675 | 556 |
| 8:00 | 1116 | 1003 | 1022 | 1068 | 1074 | 508 | 364 | 1057 | 879 |
| 9:00 | 872 | 817 | 804 | 871 | 885 | 799 | 591 | 850 | 806 |
| 10:00 | 808 | 770 | 716 | 801 | 838 | 952 | 684 | 787 | 796 |
| 11:00 | 730 | 811 | 744 | 786 | 951 | 910 | 792 | 804 | 818 |
| 12:00 | 740 | 760 | 728 | 798 | 859 | 830 | 787 | 777 | 786 |
| 13:00 | 819 | 733 | 788 | 715 | 904 | 735 | 755 | 792 | 778 |
| 14:00 | 842 | 801 | 864 | 868 | 949 | 760 | 762 | 865 | 835 |
| 15:00 | 1035 | 1063 | 1104 | 1131 | 1125 | 677 | 679 | 1092 | 973 |
| 16:00 | 1079 | 1058 | 1043 | 1163 | 1145 | 659 | 613 | 1098 | 966 |
| 17:00 | 987 | 942 | 1037 | 1044 | 1006 | 560 | 545 | 1003 | 874 |
| 18:00 | 540 | 532 | 595 | 642 | 590 | 476 | 360 | 580 | 534 |
| 19:00 | 312 | 354 | 343 | 365 | 329 | 222 | 256 | 341 | 312 |
| 20:00 | 248 | 243 | 261 | 278 | 224 | 199 | 142 | 251 | 228 |
| 21:00 | 198 | 124 | 195 | 177 | 217 | 147 | 121 | 182 | 168 |
| 22:00 | 93 | 84 | 117 | 109 | 158 | 146 | 73 | 112 | 111 |
| 23:00 | 73 | 51 | 52 | 49 | 77 | 96 | 38 | 60 | 62 |
| Total | 11924 | 11542 | 11880 | 12327 | 12855 | 9412 | 8117 | 12106 | 11151 |


| $7-19$ | 10293 | 9927 | 10104 | 10552 | 11016 | 8162 | 7153 | 10378 | 9601 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $6-22$ | 11426 | 11015 | 11339 | 11771 | 12195 | 8863 | 7802 | 11549 | 10630 |
| $6-24$ | 11592 | 11150 | 11508 | 11929 | 12430 | 9105 | 7913 | 11722 | 10804 |
| $0-24$ | 11924 | 11542 | 11880 | 12327 | 12855 | 9412 | 8117 | 12106 | 11151 |


| Job No | Q2118 - Tamworth |  |
| :--- | :--- | :--- |
| Client | TTPP |  |
| Site | Duri Road (South of Bylong St) |  |
| Location | Tamworth |  |
| Site No | 7 |  |
| Start Date | 27-Jun-18 |  |
| Description | Volume Summary |  |
| Direction | Combined |  |
|  |  |  |


| Hour <br> Starting | Day of Week |  |  |  |  |  |  | W'Day Ave 4102 | 7 Day <br> Ave <br> 3716 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Mon | Tue | Wed | Thu | Fri | Sat | Sun |  |  |
|  | 2-Jul | 3 -Jul | 27-Jun | 28-Jun | 29-Jun | 30-Jun | 1-Jul |  |  |
| AM Peak | 364 | 347 | 393 | 383 | 343 | 289 | 227 |  |  |
| PM Peak | 342 | 334 | 356 | 383 | 390 | 251 | 247 |  |  |
| 0:00 | 9 | 11 | 16 | 16 | 15 | 15 | 25 | 13 | 15 |
| 1:00 | 9 | 8 | 10 | 9 | 7 | 14 | 15 | 9 | 10 |
| 2:00 | 11 | 19 | 14 | 16 | 14 | 13 | 8 | 15 | 14 |
| 3:00 | 14 | 17 | 22 | 21 | 25 | 16 | 8 | 20 | 18 |
| 4:00 | 33 | 27 | 37 | 47 | 41 | 15 | 15 | 37 | 31 |
| 5:00 | 99 | 84 | 111 | 77 | 86 | 38 | 27 | 91 | 75 |
| 6:00 | 179 | 204 | 216 | 175 | 167 | 59 | 45 | 188 | 149 |
| 7:00 | 289 | 287 | 281 | 304 | 274 | 88 | 51 | 287 | 225 |
| 8:00 | 364 | 347 | 393 | 383 | 343 | 178 | 131 | 366 | 306 |
| 9:00 | 298 | 240 | 288 | 301 | 274 | 281 | 155 | 280 | 262 |
| 10:00 | 269 | 249 | 256 | 290 | 285 | 289 | 194 | 270 | 262 |
| 11:00 | 242 | 246 | 260 | 238 | 299 | 279 | 227 | 257 | 256 |
| 12:00 | 242 | 228 | 228 | 213 | 289 | 238 | 191 | 240 | 233 |
| 13:00 | 265 | 243 | 250 | 257 | 308 | 237 | 241 | 265 | 257 |
| 14:00 | 247 | 272 | 303 | 324 | 388 | 251 | 247 | 307 | 290 |
| 15:00 | 301 | 304 | 321 | 323 | 390 | 246 | 228 | 328 | 302 |
| 16:00 | 342 | 334 | 352 | 383 | 378 | 218 | 214 | 358 | 317 |
| 17:00 | 331 | 315 | 356 | 324 | 340 | 168 | 175 | 333 | 287 |
| 18:00 | 163 | 159 | 178 | 174 | 186 | 126 | 94 | 172 | 154 |
| 19:00 | 86 | 69 | 80 | 98 | 112 | 83 | 75 | 89 | 86 |
| 20:00 | 68 | 75 | 52 | 70 | 77 | 42 | 58 | 68 | 63 |
| 21:00 | 39 | 43 | 45 | 43 | 70 | 42 | 33 | 48 | 45 |
| 22:00 | 33 | 23 | 35 | 24 | 61 | 52 | 24 | 35 | 36 |
| 23:00 | 21 | 25 | 24 | 22 | 39 | 22 | 12 | 26 | 24 |
| Total | 3954 | 3829 | 4128 | 4132 | 4468 | 3010 | 2493 | 4102 | 3716 |


| $7-19$ | 3353 | 3224 | 3466 | 3514 | 3754 | 2599 | 2148 | 3462 | 3151 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $6-22$ | 3725 | 3615 | 3859 | 3900 | 4180 | 2825 | 2359 | 3856 | 3495 |
| $6-24$ | 3779 | 3663 | 3918 | 3946 | 4280 | 2899 | 2395 | 3917 | 3554 |
| $0-24$ | 3954 | 3829 | 4128 | 4132 | 4468 | 3010 | 2493 | 4102 | 3716 |


| Job No | Q2118- Tamworth |  |
| :--- | :--- | :--- |
| Client | TTPP |  |
| Site | Goonoo Goonoo Rd (North of Burgmans Lane) |  |
| Location | Tamworth |  |
| Site No | 8 |  |
| Start Date | 27-Jun-18 |  |
| Description | Volume Summary |  |
| Direction | Combined |  |
|  |  |  |


| Hour <br> Starting | Day of Week |  |  |  |  |  |  | W'Day Ave 6793 | 7 Day Ave 6619 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Mon | Tue | Wed | Thu | Fri | Sat | Sun |  |  |
|  | 2-Jul | 3 -Jul | 27-Jun | 28-Jun | 29-Jun | 30-Jun | 1-Jul |  |  |
| AM Peak | 544 | 544 | 532 | 564 | 554 | 573 | 505 |  |  |
| PM Peak | 543 | 546 | 556 | 584 | 662 | 608 | 546 |  |  |
| 0:00 | 14 | 24 | 36 | 36 | 35 | 45 | 40 | 29 | 33 |
| 1:00 | 15 | 21 | 18 | 18 | 21 | 26 | 17 | 19 | 19 |
| 2:00 | 17 | 27 | 11 | 9 | 23 | 18 | 22 | 17 | 18 |
| 3:00 | 22 | 29 | 26 | 33 | 29 | 20 | 11 | 28 | 24 |
| 4:00 | 46 | 39 | 60 | 48 | 65 | 28 | 22 | 52 | 44 |
| 5:00 | 123 | 115 | 100 | 108 | 118 | 77 | 38 | 113 | 97 |
| 6:00 | 208 | 224 | 220 | 214 | 219 | 107 | 81 | 217 | 182 |
| 7:00 | 359 | 367 | 341 | 348 | 355 | 215 | 146 | 354 | 304 |
| 8:00 | 544 | 544 | 532 | 564 | 554 | 420 | 329 | 548 | 498 |
| 9:00 | 531 | 406 | 446 | 460 | 477 | 517 | 385 | 464 | 460 |
| 10:00 | 424 | 374 | 429 | 444 | 494 | 511 | 492 | 433 | 453 |
| 11:00 | 453 | 404 | 416 | 433 | 448 | 573 | 505 | 431 | 462 |
| 12:00 | 473 | 409 | 398 | 417 | 504 | 608 | 542 | 440 | 479 |
| 13:00 | 383 | 415 | 384 | 468 | 549 | 495 | 511 | 440 | 458 |
| 14:00 | 418 | 436 | 436 | 487 | 586 | 519 | 541 | 473 | 489 |
| 15:00 | 502 | 537 | 540 | 558 | 662 | 480 | 546 | 560 | 546 |
| 16:00 | 518 | 531 | 541 | 584 | 662 | 447 | 427 | 567 | 530 |
| 17:00 | 543 | 546 | 556 | 581 | 626 | 455 | 379 | 570 | 527 |
| 18:00 | 357 | 320 | 328 | 400 | 454 | 323 | 283 | 372 | 352 |
| 19:00 | 211 | 214 | 202 | 241 | 258 | 201 | 208 | 225 | 219 |
| 20:00 | 161 | 161 | 171 | 165 | 225 | 136 | 128 | 177 | 164 |
| 21:00 | 88 | 136 | 128 | 130 | 180 | 145 | 79 | 132 | 127 |
| 22:00 | 66 | 63 | 87 | 72 | 144 | 105 | 59 | 86 | 85 |
| 23:00 | 42 | 51 | 35 | 44 | 61 | 70 | 41 | 47 | 49 |
| Total | 6518 | 6393 | 6441 | 6862 | 7749 | 6541 | 5832 | 6793 | 6619 |


| $7-19$ | 5505 | 5289 | 5347 | 5744 | 6371 | 5563 | 5086 | 5651 | 5558 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $6-22$ | 6173 | 6024 | 6068 | 6494 | 7253 | 6152 | 5582 | 6402 | 6249 |
| $6-24$ | 6281 | 6138 | 6190 | 6610 | 7458 | 6327 | 5682 | 6535 | 6384 |
| $0-24$ | 6518 | 6393 | 6441 | 6862 | 7749 | 6541 | 5832 | 6793 | 6619 |


| Job No | Q2118 - Tamworth |  |
| :--- | :--- | :--- |
| Client | TTPP |  |
| Site | Appleby Lane (East of Oxley Highway) |  |
| Location | Tamworth |  |
| Site No | 9 |  |
| Start Date | 27-Jun-18 |  |
| Description | Volume Summary |  |
| Direction | Combined |  |


| Hour <br> Starting | Day of Week |  |  |  |  |  |  | W'Day Ave 535 | 7 Day Ave 509 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Mon | Tue | Wed | Thu | Fri | Sat | Sun |  |  |
|  | 2-Jul | 3-Jul | 27-Jun | 28-Jun | 29-Jun | 30-Jun | 1-Jul |  |  |
| AM Peak | 48 | 46 | 51 | 48 | 49 | 32 | 40 |  |  |
| PM Peak | 48 | 52 | 55 | 52 | 51 | 41 | 64 |  |  |
| 0:00 | 1 | 0 | 0 | 1 | 0 | 3 | 3 | 0 | 1 |
| 1:00 | 0 | 2 | 0 | 0 | 1 | 1 | 0 | 1 | 1 |
| 2:00 | 0 | 0 | 2 | 0 | 1 | 1 | 1 | 1 | 1 |
| 3:00 | 6 | 1 | 3 | 3 | 4 | 1 | 0 | 3 | 3 |
| 4:00 | 13 | 16 | 10 | 9 | 9 | 5 | 3 | 11 | 9 |
| 5:00 | 24 | 15 | 18 | 10 | 13 | 10 | 3 | 16 | 13 |
| 6:00 | 18 | 25 | 26 | 29 | 23 | 9 | 10 | 24 | 20 |
| 7:00 | 48 | 46 | 51 | 48 | 49 | 21 | 13 | 48 | 39 |
| 8:00 | 40 | 45 | 47 | 36 | 38 | 32 | 40 | 41 | 40 |
| 9:00 | 37 | 36 | 38 | 32 | 27 | 26 | 38 | 34 | 33 |
| 10:00 | 26 | 28 | 38 | 26 | 27 | 30 | 29 | 29 | 29 |
| 11:00 | 23 | 30 | 38 | 38 | 23 | 24 | 29 | 30 | 29 |
| 12:00 | 28 | 34 | 30 | 28 | 31 | 32 | 43 | 30 | 32 |
| 13:00 | 22 | 30 | 27 | 23 | 31 | 26 | 64 | 27 | 32 |
| 14:00 | 40 | 43 | 41 | 32 | 34 | 34 | 48 | 38 | 39 |
| 15:00 | 40 | 47 | 36 | 52 | 43 | 38 | 43 | 44 | 43 |
| 16:00 | 48 | 52 | 55 | 50 | 51 | 41 | 42 | 51 | 48 |
| 17:00 | 43 | 42 | 41 | 43 | 50 | 28 | 22 | 44 | 38 |
| 18:00 | 31 | 28 | 23 | 30 | 35 | 12 | 27 | 29 | 27 |
| 19:00 | 13 | 11 | 8 | 17 | 7 | 11 | 9 | 11 | 11 |
| 20:00 | 12 | 10 | 8 | 13 | 11 | 7 | 1 | 11 | 9 |
| 21:00 | 3 | 5 | 2 | 4 | 8 | 9 | 10 | 4 | 6 |
| 22:00 | 4 | 4 | 2 | 5 | 11 | 2 | 4 | 5 | 5 |
| 23:00 | 0 | 1 | 1 | 1 | 0 | 6 | 0 | 1 | 1 |
| Total | 520 | 551 | 545 | 530 | 527 | 409 | 482 | 535 | 509 |


| $7-19$ | 426 | 461 | 465 | 438 | 439 | 344 | 438 | 446 | 430 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $6-22$ | 472 | 512 | 509 | 501 | 488 | 380 | 468 | 496 | 476 |
| $6-24$ | 476 | 517 | 512 | 507 | 499 | 388 | 472 | 502 | 482 |
| $0-24$ | 520 | 551 | 545 | 530 | 527 | 409 | 482 | 535 | 509 |




MATRIX

Day/Date
Description : Classified Intersection Count
: Intersection Diagram

$\longleftarrow 2$
Day/Date - Wed, 27thun 2018
Description : Classified Intersection Count : Intersection Diagram
Hour Starting
Hour Starting

| Wallamore Rd |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Total |  |  |  |  |  | $\begin{gathered} \text { Total } \\ \text { Southbd } \end{gathered}$ |
| 99 $100 \%$ | Selected Hour \& Vehicle Type |  | 0 <br> $0 \%$ | 23 <br> $18 \%$ | 102 <br> $82 \%$ |  |
| $\begin{aligned} & 21 \\ & 21 \% \end{aligned}$ | AM Peak | $\begin{aligned} & \text { (Vol) } \\ & \text { (\%) } \end{aligned}$ | 0 $0 \%$ | 8 <br> $16 \%$ | 41 <br> $84 \%$ | 49 $39 \%$ |
| $$ | PM Peak |  | $\begin{gathered} \begin{array}{c} 0 \\ 0 \% \\ 0 \% \end{array} \\ \hline \end{gathered}$ | $\begin{gathered} \begin{array}{c} 5 \\ 19 \% \end{array} \\ ]_{1} \end{gathered}$ | $\begin{gathered} \begin{array}{c} 22 \\ 81 \% \\ 1 \\ \hline \end{array} \end{gathered}$ | $\begin{gathered} \begin{array}{c} 27 \\ \text { 23\% } \\ \nabla \end{array} \end{gathered}$ |
|  |  |  | 90 | 9 | 8 |  |

$N$

MATRIX
Day/Date : Wed, 27th Jun 2018
Description : Classified Intersection Count
: Intersection Diagram
Hour Starting
Hour Starting


MATRIX




## MATRIK



## Appendix B

Road Crash Summary Analysis Tables

Oxley Highway Crash Summary (Appleby Lane to Duri Road) 1 July 2012 to 30 June 2017

|  |  | Multiple Vehicles |  |  |  |  | Single Vehicle |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & \text { 든 } \\ & \text { 흔 } \\ & \frac{1}{0} \\ & \dot{0} \end{aligned}$ |  | Opposing Directions |  | U-turn/Parking |  | $\begin{aligned} & \text { 등 } \\ & \text { ᄃ } \\ & \hline \end{aligned}$ |  | 0 <br> 3 <br> 3 <br> 0 <br> 0 <br> 0 <br> $\frac{5}{0}$ <br> 0 <br>  |  | 흥 |
| Total Crashes | - | 7 | 3 | 12 | - | - | 2 | 11 | 2 | - | 37 |


| Crash Location Type |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2-way undivided road | - | - | 2 | 4 | - | - | 2 | 8 | 2 | - | 18 |
| Roundabout | - | 1 | - | - | - | - | - | 2 | - | - | 3 |
| Cross Intersection | - | 1 | - | - | - | - | - | - | - | - | 1 |
| T-intersection | - | 5 | 1 | 8 | - | - | - | 1 | - | - | 15 |

Severity of Crash

| Fatal | - | - | 1 | - | - | - | - | - | - | - | 1 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Serious Injury | - | 1 | 1 | 1 | - | - | - | 2 | - | - | 5 |
| Moderate Injury | - | 3 | 1 | 8 | - | - | - | 1 | 1 | - | 14 |
| Non-injury | - | 3 | - | 3 | - | - | 2 | 8 | 1 | - | 17 |

## Weather Conditions

| Fine | - | 7 | 1 | 11 | - | - | 1 | 8 | 2 | - | 30 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Overcast | - | - | - | - | - | - | - | 2 | - | - | 2 |
| Raining | - | - | 2 | 1 | - | - | 1 | 1 | - | - | 5 |

## Road Surface Condition

| Dry | - | 7 | 1 | 11 | - | - | 1 | 9 | 2 | - | 31 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Wet | - | - | 2 | 1 | - | - | 1 | 2 | - | - | 6 |

Speed Limit

| $40 \mathrm{~km} / \mathrm{h}$ | - | - | - | 1 | - | - | - | 1 | - | - | 2 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $50 \mathrm{~km} / \mathrm{h}$ | - | 1 | - | 1 | - | - | - | - | - | - | 2 |
| $60 \mathrm{~km} / \mathrm{h}$ | - | 2 | - | 7 | - | - | - | 3 | - | - | 12 |
| $70 \mathrm{~km} / \mathrm{h}$ | - | 1 | 1 | 3 | - | - | - | - | - | - | 5 |
| $80 \mathrm{~km} / \mathrm{h}$ | - | 1 | - | - | - | - | 1 | 1 | - | - | 3 |
| $100 \mathrm{~km} / \mathrm{h}$ | - | 2 | 2 | - | - | - | 1 | 6 | 2 | - | 13 |

Key Vehicle Type ${ }^{A}$

| Motorcycle | - | - | - | 1 | - | - | - | - | - | - | 1 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Car, 4WD, Station Wagon | - | 4 | 3 | 9 | - | - | 2 | 7 | 1 | - | 26 |
| Rigid Truck | - | 2 | - | 2 | - | - | - | 3 | 1 | - | 8 |
| Articulated | - | 1 | - | - | - | - | - | 1 | - | - | 2 |

[^0]Oxley Highway Crash Summary (Duri Road to Marius Street) 1 July 2012 to 30 June 2017

|  | 든은0000 | Multiple Vehicles |  |  |  |  | Single Vehicle |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | səบวDoıdd $\forall$ łuәวロ!p $\forall$ |  |  | 은 른 은 들 $\frac{1}{j}$ | $\begin{aligned} & \text { ㅇ } \\ & \text { 든 } \\ & \frac{0}{ㄴ} \\ & 0 \\ & 0 \end{aligned}$ |  |  | 0 <br> 3 <br> 3 <br> 0 <br> 0 <br> 0 <br> $\frac{5}{0}$ <br> 0 <br>  | Miscellaneous | 흥 |
| Total Crashes | - | 12 | 11 | 16 | 4 | - | - | 5 | 2 | - | 50 |


| Crash Location Type |  | - | - | 3 | 1 | - | - | 1 | 1 | - | 6 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Divided road | - | - | - | - | - | - | - | - | 1 | - | 1 |
| 2-way undivided road | - | - | 1 | 2 | 0 | - | - | 1 | - | - | 4 |
| T-intersection | - | 8 | 9 | 5 | 2 | - | - | - | - | - | 24 |
| Cross Intersection | - | 4 | 1 | 6 | 1 | - | - | 3 | - | - | 15 |
| Roundabout |  |  |  |  |  |  |  |  |  |  |  |

Severity of Crash

| Serious Injury | - | 1 | - | - | - | - | - | - | - | - | 1 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Moderate Injury | - | 4 | 5 | 6 | 3 | - | - | 3 | - | - | 21 |
| Minor Injury | - | 1 | - | 2 | - | - | - | - | - | - | 3 |
| Non-injury | - | 6 | 6 | 8 | 1 | - | - | 2 | 2 | - | 25 |

Weather Conditions

| Fine | - | 12 | 10 | 14 | 4 | - | - | 5 | - | - | 45 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Overcast | - | - | 1 | - | - | - | - | - | - | - | 1 |
| Raining | - | - | - | 2 | - | - | - | - | 2 | - | 4 |

Road Surface Condition

| Dry | - | 12 | 10 | 13 | 4 | - | - | 5 | - | - | 44 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Wet | - | - | 1 | 3 | - | - | - | - | 2 | - | 6 |

Speed Limit

| $50 \mathrm{~km} / \mathrm{h}$ | - | 10 | 9 | 11 | 3 | - | - | 4 | 1 | - | 38 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $60 \mathrm{~km} / \mathrm{h}$ | - | 2 | 2 | 5 | 1 | - | - | 1 | 1 | - | 12 |

Key Vehicle Type ${ }^{A}$

| Motorcycle/Pedal Cycle | - | - | - | - | 2 | - | - | 1 | - | - | 3 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Car, 4WD, Station Wagon | - | 11 | 9 | 12 | 1 | - | - | 4 | 2 | - | 39 |
| Rigid Truck | - | 1 | 2 | 3 | 1 | - | - | - | - | - | 7 |
| Articulated | - | - | - | 1 | - | - | - | - | - | - | 1 |

[^1]Wallamore Road Crash Summary 1 July 2012 to 30 June 2017

|  | 든흔$\frac{0}{8}$0 | Multiple Vehicles |  |  |  |  | Single Vehicle |  |  |  | $\overline{\bar{O}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  | $\begin{aligned} & \text { 듬 } \\ & \text { ᄃ } \\ & \hline \end{aligned}$ |  | 0 <br> 3 <br> 3 <br> 0 <br> 0 <br> 0 <br> 든 <br> 0 <br> 4 <br> 0 |  |  |
| Total Crashes | - | - | 1 | 3 | 1 | - | 1 | 3 | 2 | - | 11 |

Crash Location Type

| Divided road |  | - | - | - | - | - | - | 1 | - | - | 1 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2-way undivided road | - | - | 1 | 2 | 1 | - | 1 | 1 | 2 | - | 8 |
| T-intersection | - | - | - | 1 | - | - | - | 1 | - | - | 2 |

Severity of Crash

| Serious Injury | - | - | 1 | 1 | - | - | - | - | 1 | - | 3 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Moderate Injury | - | - | - | 1 | - | - | - | 1 | - | - | 2 |
| Minor Injury | - | - | - | - | - | - | 1 | - | - | - | 1 |
| Non-injury | - | - | - | 1 | 1 | - | - | 2 | 1 | - | 5 |

Weather Conditions

| Fine | - | - | 1 | 2 | 1 | - | 1 | 1 | 2 | - | 8 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fog or Mist | - | - | - | - | - | - | - | 1 | - | - | 1 |
| Raining | - | - | - | 1 | - | - | - | 1 | - | - | 2 |

Road Surface Condition

| Dry | - | - | 1 | 2 | 1 | - | 1 | - | 2 | - | 7 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Wet | - | - | - | 1 | - | - | - | 3 | - | - | 4 |

Speed Limit

| $60 \mathrm{~km} / \mathrm{h}$ | - | - | - | 1 | - | - | - | - | - | - | 1 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $70 \mathrm{~km} / \mathrm{h}$ | - | - | - | - | - | - | - | 1 | - |  | 1 |
| $80 \mathrm{~km} / \mathrm{h}$ | - | - | 1 | 2 | - | - | - | 1 | - |  | 4 |
| $100 \mathrm{~km} / \mathrm{h}$ | - | - | - | - | 1 | - | 1 | 1 | 2 | - | 5 |

Key Vehicle Type ${ }^{\text {A }}$

| Motorcycle | - | - | - | - | - | - | 1 | - | - | - | 1 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Car, 4WD, Station Wagon | - | - | 1 | 3 | 1 | - | - | 2 | - | - | 7 |
| Rigid Truck | - | - | - | - | - | - | - | 1 | 1 | - | 2 |
| Articulated | - | - | - | - | - | - | - | - | 1 | - | 1 |

[^2]Duri Road (Oxley Highway to Burgmanns Lane) Crash Summary 1 July 2012 to 30 June 2017

|  | $\begin{aligned} & \text { 든 } \\ & \text { 는 } \\ & \frac{0}{0} \\ & 0 \end{aligned}$ | Multiple Vehicles |  |  |  |  | Single Vehicle |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Adjacent Approaches |  |  |  | $\begin{aligned} & \text { 은 } \\ & \text { 든 } \\ & \text { 흥 } \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & \text { 듬 } \\ & \text { ᄃ } \\ & \hline \end{aligned}$ |  |  |  | $\stackrel{\overline{0}}{\square}$ |
| Total Crashes | 2 | 5 | - | 3 | 1 | - | - | 8 | 4 | - | 23 |

Crash Location Type

| Divided road | - | - | - | - | - | - | - | 1 | - | - | 1 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2-way undivided road | 1 | - | - | 1 | - | - | - | 2 | 2 | - | 6 |
| Roundabout | 1 | - | - | - | - | - | - | 4 | 1 | - | 6 |
| T-intersection | - | 5 | - | 2 | 1 | - | - | 1 | 1 | - | 10 |

Severity of Crash

| Serious Injury | - | 1 | - | - | - | - | - | - | 1 | - | 2 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Moderate Injury | 2 | 3 | - | 1 | - | - | - | 4 | 1 | - | 11 |
| Minor Injury | - | - | - | - | - | - | - | 1 | - | - | 1 |
| Non-injury | - | 1 | - | 2 | 1 | - | - | 3 | 2 | - | 9 |

Weather Conditions

| Fine | 2 | 4 | - | 3 | 1 | - | - | 5 | 4 | - | 19 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Overcast | - | - | - | - | - | - | - | 2 | - | - | 2 |
| Fog or Mist | - | - | - | - | - | - | - | 1 | - | - | 1 |
| Raining | - | 1 | - | - | - | - | - | - | - | - | 1 |

Road Surface Condition

| Dry | 2 | 4 | - | 3 | 1 | - | - | 6 | 4 | - | 20 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Wet | - | 1 | - | - | - | - | - | 2 | - | - | 3 |


| Speed Limit |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $40 \mathrm{~km} / \mathrm{h}$ | - | 1 | - | - | - | - | - | - | - | - | 1 |
| $50 \mathrm{~km} / \mathrm{h}$ | - | - | - | - | - | - | - | - | 1 | - | 1 |
| $60 \mathrm{~km} / \mathrm{h}$ | 1 | 2 | - | 2 | - | - | - | 6 | 1 | - | 12 |
| $100 \mathrm{~km} / \mathrm{h}$ | 1 | 2 | - | 1 | 1 | - | - | 2 | 2 | - | 9 |

Key Vehicle Type ${ }^{A}$

| Motorcycle/moped | - | - | - | - | - | - | - | 1 | - | - | 1 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Car, 4WD, Station Wagon | 2 | 4 | - | 2 | - | - | - | 6 | 3 | - | 17 |
| Rigid Truck | - | 1 | - | - | - | - | - | - | 1 | - | 2 |
| Articulated | - | - | - | 1 | - | - | - | 1 | - | - | 2 |
| Unknown | - | - | - | - | 1 | - | - | - | - | - | 1 |

a The first vehicle identified in multiple vehicle crashes.

Dampier Street - Jewry Street Crash Summary 1 July 2012 to 30 June 2017


Severity of Crash

| Serious Injury | - | - | 1 | 1 | - | - | - | 1 | - | - | 3 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Moderate Injury | - | - | - | 5 | - | - | - | 1 | - | - | 6 |
| Non-injury | - | - | - | 3 | - | - | - | - | - | - | 3 |

Weather Conditions

| Fine | - | - | - | 9 | - | - | - | 1 | - | - | 10 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Overcast | - | - | 1 | - | - | - | - | - | - | - | 1 |
| Raining | - | - | - | - | - | - | - | 1 | - | - | 1 |

Road Surface Condition

| Dry | - | - | 1 | 9 | - | - | - | 1 | - | - | 11 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Wet | - | - | - | - | - | - | - | 1 | - | - | 1 |


| Speed Limit |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $50 \mathrm{~km} / \mathrm{h}$ | - | - | - | 1 | - | - | - | - | - | - | 1 |
| $60 \mathrm{~km} / \mathrm{h}$ | - | - | 1 | 8 | - | - | - | 2 | - | - | 11 |

Key Vehicle Type ${ }^{\text {A }}$

| Motorcycle | - | - | - | - | - | - | - | 1 | - | - | 1 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Car, 4WD, Station Wagon | - | - | - | 3 | - | - | - | 1 | - | - | 4 |
| Rigid Truck | - | - | 1 | 4 | - | - | - | - | - | - | 5 |
| Articulated | - | - | - | 2 | - | - | - | - | - | - | 2 |

[^3]transport planning

Ebsworth Street Crash Summary 1 July 2012 to 30 June 2017


## Severity of Crash

| Serious Injury | - | - | - | - | - | - | - | - | 1 | - | 1 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Moderate Injury | - | 1 | - | 2 | - | - | - | - | - | - | 3 |
| Non-injury | - | - | - | 1 | - | - | - | 1 | - | - | 2 |

Weather Conditions

| Fine | - | 1 | - | 3 | - | - | - | 1 | 1 | - | 6 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

Road Surface Condition

| Dry | - | 1 | - | 3 | - | - | - | 1 | 1 | - | 6 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

Speed Limit

| $50 \mathrm{~km} / \mathrm{h}$ | - | 1 | - | 1 | - | - | - | 1 | 1 | - | 4 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $60 \mathrm{~km} / \mathrm{h}$ | - | - | - | 2 | - | - | - | - | - | - | 2 |

Key Vehicle Type ${ }^{A}$

| Motorcycle | - | - | - | - | - | - | - | - | 1 | - | 1 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Car, 4WD, Station Wagon | - | 1 | - | 3 | - | - | - | 1 | - | - | 5 |

A The first vehicle identified in multiple vehicle crashes.

Manilla Road Route Crash Summary 1 July 2012 to 30 June 2017

|  | $\begin{aligned} & \text { 든 } \\ & \text { 흔 } \\ & \frac{0}{0} \\ & 0 \end{aligned}$ | Multiple Vehicles |  |  |  |  | Single Vehicle |  |  |  | 흔 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\text { sə૫כDoıdd } \forall \text { łuəכD!p } \forall$ | suo!†วəఎ! бu!soddo |  | U-łurn/Parking | $\begin{aligned} & \text { 은 } \\ & \text { 든 } \\ & \frac{0}{ㄴ} \\ & 0 \\ & 0 \end{aligned}$ |  |  | $\begin{aligned} & 0 \\ & 2 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & \frac{1}{0} \\ & 0 \\ & \hline 0 \end{aligned}$ |  |  |
| Total Crashes | - | 12 | - | 9 | 1 | - | 1 | 4 | 1 | - | 28 |
| Crash Location Type |  |  |  |  |  |  |  |  |  |  |  |
| Divided road | - | - | - | 2 | - | - | - | - | - | - | 2 |
| 2-way undivided road | - | - | - | 4 | 1 | - | 1 | 1 | - | - | 7 |
| T-intersection | - | 5 | - | 2 | - | - | - | 3 | - | - | 10 |
| Cross intersection | - | 4 | - | - | - | - | - | - | - | - | 4 |
| Roundabout | - | 3 | - | 1 | - | - | - | - | 1 | - | 5 |
| Severity of Crash |  |  |  |  |  |  |  |  |  |  |  |
| Serious Injury | - | - | - | - | - | - | - | 1 | - | - | 1 |
| Moderate Injury | - | 9 | - | 4 | 1 | - | 1 | - | - | - | 15 |
| Minor injury | - | - | - | 1 | - | - | - | - | - | - | 1 |
| Non-injury | - | 3 | - | 4 | - | - | - | 3 | 1 | - | 11 |

Weather Conditions

| Fine | - | 10 | - | 6 | 1 | - | 1 | 3 | 1 | - | 22 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Overcast | - | - | - | 2 | - | - | - | 1 | - | - | 3 |
| Raining | - | 10 | - | 6 | 1 | - | 1 | 3 | 1 | - | 22 |

## Road Surface Condition

| Dry | - | 10 | - | 7 | 1 | - | 1 | 4 | - | - | 23 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Wet | - | 2 | - | 2 | - | - | - | - | 1 | - | 5 |

Speed Limit

| $40 \mathrm{~km} / \mathrm{h}$ | - | 1 | - | 1 | - | - | - | - | - | - | 2 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $50 \mathrm{~km} / \mathrm{h}$ | - | 1 | - | - | 1 | - | - | - | - | - | 2 |
| $60 \mathrm{~km} / \mathrm{h}$ | - | 10 | - | 8 | - | - | 1 | 4 | 1 | - | 24 |

Key Vehicle Type ${ }^{A}$

| Motorcycle/Pedal cycle | - | 1 | - | - | 1 | - | 1 | 1 | - | - | 4 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Car, 4WD, Station Wagon | - | 9 | - | 6 | - | - | - | 3 | 1 | - | 19 |
| Rigid Truck | - | 2 | - | 3 | - | - | - | - | - | - | 5 |

[^4]Marius Street Crash Summary 1 July 2012 to 30 June 2017

|  | 든을©00 | Multiple Vehicles |  |  |  |  | Single Vehicle |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | sə૫วDoıdd $\forall$ łuəวロ!pヲ |  | $\begin{aligned} & \text { co } \\ & \text { 은 } \\ & 0 . \overline{0} \\ & 0 \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & \text { 온 } \\ & \text { 듬 } \\ & \frac{2}{2} \\ & \frac{5}{2} \\ & \frac{1}{3} \end{aligned}$ | $\begin{aligned} & \text { 이 } \\ & \text { 든 } \\ & \text { ㅁㄴㅇ } \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & \text { ع } 10 \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ |  | 0 <br> 3 <br> 3 <br> 0 <br> 0 <br> 든 <br> 0 <br> 0 <br> 4 <br> 0 | n <br> 0 <br> 0 <br> 0 <br> $\frac{0}{0}$ <br> $\overline{0}$ <br> $U$ <br>  | 흥 |
| Total Crashes | - | 2 | 4 | 10 | 1 | - | - | 2 | 2 | 1 | 22 |

Crash Location Type

| 2-way undivided road | - | - | - | 2 | - | - | - | 1 | - | - | 3 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T-intersection | - | - | - | 1 | - | - | - | - | - | - | 1 |
| Cross intersection | - | 1 | 1 | 5 | - | - | - | - | - | - | 7 |
| Roundabout | - | 1 | 3 | 1 | - | - | - | 1 | 1 | 1 | 8 |

Severity of Crash

| Serious Injury | - | 1 | - | - | - | - | - | - | - | - | 1 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Moderate Injury | - | 1 | 2 | 3 | 1 | - | - | 2 | 1 | 1 | 11 |
| Minor Injury | - | - | 1 | 4 | - | - | - | - | - | - | 5 |
| Non-injury | - | - | 1 | 3 | - | - | - | - | 1 | - | 5 |

Weather Conditions

| Fine | - | 2 | 3 | 9 | 1 | - | - | 2 | 2 | 1 | 20 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Overcast | - | - | 1 | - | - | - | - | - | - | - | 1 |
| Raining | - | - | - | 1 | - | - | - | - | - | - | 1 |

Road Surface Condition

| Dry | - | 2 | 4 | 9 | 1 | - | - | 2 | 2 | 1 | 21 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Wet | - | - | - | 1 | - | - | - | - | - | - | 1 |

Speed Limit

| $50 \mathrm{~km} / \mathrm{h}$ | - | - | 1 | - | - | - | - | 1 | - | - | 2 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $60 \mathrm{~km} / \mathrm{h}$ | - | 2 | 3 | 5 | 1 | - | - | - | 2 | 1 | 14 |
| $70 \mathrm{~km} / \mathrm{h}$ | - | - | - | 5 | - | - | - | 1 | - | - | 6 |

Key Vehicle Type ${ }^{A}$

| Motorcycle/Pedal cycle | - | 1 | - | 2 | - | - | - | 1 | - | - | 4 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Car, 4WD, Station Wagon | - | 1 | 4 | 5 | 1 | - | - | 1 | - | - | 12 |
| Rigid Truck/Bus | - | - | - | 3 | - | - | - | - | - | 1 | 4 |
| Articulated | - | - | - | - | - | - | - | - | 1 | - | 1 |
| Unknown | - | - | - | - | - | - | - | - | 1 | - | 1 |

A The first vehicle identified in multiple vehicle crashes.

## Appendix C

## SIDRA Output Summaries

## MOVEMENT SUMMARY

Site: 101 [AM Ex Goddard - Armstrong]
Goddard Lane and Armstrong Street

## Surveyed AM Peak

7:45am to 8:45am
Site Category: (None)
Giveway / Yield (Two-Way)

Movement Performance - Vehicles


Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

SIDRA INTERSECTION 8.0 | Copyright © 2000-2018 Akcelik and Associates Pty Ltd | sidrasolutions.com
Organisation: TTPP - THE TRANSPORT PLANNING PARTNERSHIP | Processed: Friday, 28 September 2018 12:10:17 PM
Project: E:ITTPP Projects Local CopylSidra\18089\18089_181003_Oakburn Processing Plant.sip8

## MOVEMENT SUMMARY

## $\nabla$ Site: 101 [Site AM Ex Oxley - Baiada]

## Surveyed AM Peak Hour for Site Traffic

6.15am to 7.15am

Site Category: (None)
Giveway / Yield (Two-Way)


Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## MOVEMENT SUMMARY

## $\theta$ Site: 101 [AM Ex Oxley - Duri]

Oxley Highway and Duri Road
Surveyed AM Peak
8:00am to 9:00am
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Deman <br> Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| NorthEast: Oxley Highway (NE) |  |  |  |  |  |  |  |  |  |  |  |  |
| 25 | T1 | 160 | 5.9 | 0.082 | 4.7 | LOS A | 0.0 | 0.0 | 0.00 | 0.46 | 0.00 | 55.5 |
| 26a | R1 | 261 | 4.4 | 0.211 | 8.5 | LOS A | 1.3 | 9.7 | 0.47 | 0.64 | 0.47 | 51.3 |
| Appr |  | 421 | 5.0 | 0.211 | 7.0 | LOS A | 1.3 | 9.7 | 0.29 | 0.57 | 0.29 | 52.8 |
| West: Oxley Highway (W) |  |  |  |  |  |  |  |  |  |  |  |  |
| 10a | L1 | 276 | 4.6 | 0.144 | 4.3 | LOS A | 0.0 | 0.0 | 0.00 | 0.47 | 0.00 | 55.5 |
| 12b | R3 | 232 | 12.3 | 0.227 | 11.5 | LOSA | 1.4 | 11.2 | 0.61 | 0.74 | 0.61 | 50.1 |
| Appr |  | 507 | 8.1 | 0.227 | 7.6 | LOS A | 1.4 | 11.2 | 0.28 | 0.59 | 0.28 | 52.9 |
| SouthWest: Duri Road |  |  |  |  |  |  |  |  |  |  |  |  |
| 30b | L3 | 268 | 13.7 | 0.174 | 4.2 | LOS A | 0.0 | 0.0 | 0.00 | 0.52 | 0.00 | 54.5 |
| 31 | T1 | 435 | 3.6 | 0.354 | 6.1 | LOS A | 2.4 | 17.6 | 0.53 | 0.58 | 0.53 | 53.3 |
| Approach |  | 703 | 7.5 | 0.354 | 5.4 | LOS A | 2.4 | 17.6 | 0.33 | 0.56 | 0.33 | 53.7 |
| All Vehicles |  | 1632 | 7.0 | 0.354 | 6.5 | LOS A | 2.4 | 17.6 | 0.30 | 0.57 | 0.30 | 53.2 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

[^5]
## MOVEMENT SUMMARY

## $\nabla$ Site: 101 [AM Ex Oxley - Goddard]

Oxley Hwy and Goddard Ln
Surveyed AM Peak
7:45am to 8:45am
Site Category: (None)
Giveway / Yield (Two-Way)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{ll} \text { Mov Turn } \\ \text { ID } \end{array}$ | Demano Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| SouthEast: Oxley Highway (south-east) 0.0 0 |  |  |  |  |  |  |  |  |  |  |  |
| 22 T1 | 128 | 22.1 | 0.076 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 100.0 |
| 23 R2 | 59 | 17.9 | 0.054 | 9.2 | LOS A | 0.2 | 1.7 | 0.31 | 0.63 | 0.31 | 62.3 |
| Approach | 187 | 20.8 | 0.076 | 2.9 | NA | 0.2 | 1.7 | 0.10 | 0.20 | 0.10 | 84.0 |
| NorthEast: Goddard Lane |  |  |  |  |  |  |  |  |  |  |  |
| 24 L2 | 55 | 38.5 | 0.125 | 8.7 | LOS A | 0.5 | 4.3 | 0.30 | 0.63 | 0.30 | 58.0 |
| 26 R2 | 43 | 17.1 | 0.125 | 10.8 | LOS A | 0.5 | 4.3 | 0.30 | 0.63 | 0.30 | 61.9 |
| Approach | 98 | 29.0 | 0.125 | 9.6 | LOS A | 0.5 | 4.3 | 0.30 | 0.63 | 0.30 | 59.7 |
| NorthWest: Oxley Highway (north-west) |  |  |  |  |  |  |  |  |  |  |  |
| 27 L2 | 80 | 5.3 | 0.045 | 8.8 | LOS A | 0.0 | 0.0 | 0.00 | 0.63 | 0.00 | 72.7 |
| 28 T1 | 101 | 19.8 | 0.058 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 100.0 |
| Approach | 181 | 13.4 | 0.058 | 3.9 | NA | 0.0 | 0.0 | 0.00 | 0.28 | 0.00 | 85.6 |
| All Vehicles | 466 | 19.6 | 0.125 | 4.7 | NA | 0.5 | 4.3 | 0.10 | 0.32 | 0.10 | 77.9 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Organisation: TTPP - THE TRANSPORT PLANNING PARTNERSHIP | Processed: Tuesday, 18 September 2018 5:54:09 PM
Project: E:ITTPP Projects Local CopylSidral18089\18089_181003_Oakburn Processing Plant.sip8

## MOVEMENT SUMMARY

## Site: 101 [AM Ex Oxley - Marius - Brisbane]

Oxley Highway, Marius Street and Brisbane Street
Surveyed AM Peak Hour
8:15am to 9:15am
Site Category: (None)
Signals - Fixed Time Isolated Cycle Time $=93$ seconds (Site User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Demand <br> Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| SouthEast: Marius Street (SE) |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 | L2 | 222 | 6.2 | 0.190 | 12.3 | LOS A | 3.9 | 28.7 | 0.42 | 0.69 | 0.42 | 41.6 |
| 22 | T1 | 443 | 6.4 | 0.688 | 28.4 | LOS B | 17.4 | 128.6 | 0.92 | 0.80 | 0.92 | 38.5 |
| 23 | R2 | 36 | 2.9 | 0.141 | 35.9 | LOS C | 1.3 | 9.4 | 0.81 | 0.73 | 0.81 | 34.4 |
| Appr |  | 701 | 6.2 | 0.688 | 23.7 | LOS B | 17.4 | 128.6 | 0.76 | 0.76 | 0.76 | 38.9 |
| NorthEast: Brisbane Street |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 | L2 | 104 | 3.0 | 0.483 | 40.7 | LOS C | 7.7 | 56.6 | 0.93 | 0.79 | 0.93 | 33.5 |
| 25 | T1 | 237 | 8.0 | 0.483 | 35.2 | LOS C | 7.8 | 57.7 | 0.93 | 0.78 | 0.93 | 32.4 |
| 26 | R2 | 41 | 2.6 | 0.483 | 40.7 | LOS C | 7.8 | 57.7 | 0.93 | 0.77 | 0.93 | 36.9 |
| Appr |  | 382 | 6.1 | 0.483 | 37.3 | LOS C | 7.8 | 57.7 | 0.93 | 0.78 | 0.93 | 33.3 |
| NorthWest: Marius Street (NW) |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 | L2 | 57 | 0.0 | 0.389 | 30.2 | LOS C | 8.4 | 62.5 | 0.80 | 0.70 | 0.80 | 41.3 |
| 28 | T1 | 434 | 10.0 | 0.389 | 24.8 | LOS B | 8.5 | 64.2 | 0.80 | 0.69 | 0.80 | 40.0 |
| 29 | R2 | 39 | 0.0 | 0.250 | 45.4 | LOS D | 1.7 | 11.6 | 0.92 | 0.75 | 0.92 | 28.7 |
| Appr |  | 529 | 8.2 | 0.389 | 26.9 | LOS B | 8.5 | 64.2 | 0.81 | 0.69 | 0.81 | 39.2 |
| SouthWest: Oxley Highway |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 | L2 | 43 | 2.4 | 0.096 | 34.7 | LOS C | 1.5 | 10.8 | 0.80 | 0.72 | 0.80 | 32.5 |
| 31 | T1 | 165 | 1.9 | 0.347 | 31.4 | LOS C | 6.2 | 44.5 | 0.87 | 0.71 | 0.87 | 34.8 |
| 32 | R2 | 193 | 10.9 | 0.452 | 38.2 | LOS C | 7.5 | 57.8 | 0.90 | 0.80 | 0.90 | 27.2 |
| Approach |  | 401 | 6.3 | 0.452 | 35.0 | LOS C | 7.5 | 57.8 | 0.87 | 0.75 | 0.87 | 31.0 |
| All V | icles | 2014 | 6.7 | 0.688 | 29.4 | LOS C | 17.4 | 128.6 | 0.83 | 0.75 | 0.83 | 36.2 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## $\theta$ Site: 101 [AM Ex Peel - Jewry]

Peel Street and Jewry Street
Surveyed AM Peak Hour
8:15am to 9:15am
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Turn | Deman <br> Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| SouthEast: Peel Street (SE) |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 | L2 | 307 | 9.9 | 0.501 | 11.7 | LOS A | 4.4 | 33.1 | 0.94 | 0.99 | 1.07 | 48.9 |
| 22 | T1 | 295 | 5.4 | 0.530 | 12.7 | LOS A | 4.6 | 33.9 | 0.95 | 1.03 | 1.12 | 49.5 |
| 23 | R2 | 4 | 0.0 | 0.530 | 16.5 | LOS B | 4.6 | 33.9 | 0.95 | 1.03 | 1.12 | 28.9 |
| Appro | ach | 606 | 7.6 | 0.530 | 12.2 | LOS A | 4.6 | 33.9 | 0.94 | 1.01 | 1.10 | 49.0 |
| NorthEast: Car Park |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 | L2 | 14 | 0.0 | 0.084 | 9.2 | LOS A | 0.4 | 2.7 | 0.81 | 0.81 | 0.81 | 27.3 |
| 25 | T1 | 9 | 0.0 | 0.084 | 9.2 | LOS A | 0.4 | 2.7 | 0.81 | 0.81 | 0.81 | 27.4 |
| 26 | R2 | 1 | 0.0 | 0.084 | 9.2 | LOS A | 0.4 | 2.7 | 0.81 | 0.81 | 0.81 | 27.6 |
| Appro | ach | 24 | 0.0 | 0.084 | 9.2 | LOS A | 0.4 | 2.7 | 0.81 | 0.81 | 0.81 | 27.3 |
| NorthWest: Peel Street (NW) |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 | L2 | 13 | 8.3 | 0.536 | 9.1 | LOS A | 4.4 | 31.9 | 0.75 | 0.78 | 0.81 | 28.4 |
| 28 | T1 | 525 | 3.8 | 0.768 | 9.0 | LOS A | 11.1 | 81.6 | 0.78 | 0.81 | 0.87 | 51.6 |
| 29 | R2 | 704 | 5.7 | 0.768 | 15.0 | LOS B | 11.1 | 81.6 | 0.93 | 0.93 | 1.18 | 48.2 |
| Appro | ach | 1242 | 4.9 | 0.768 | 12.4 | LOS A | 11.1 | 81.6 | 0.87 | 0.87 | 1.04 | 49.2 |
| SouthWest: Jewry Street |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 | L2 | 601 | 6.0 | 0.574 | 7.1 | LOS A | 5.3 | 38.9 | 0.75 | 0.73 | 0.77 | 52.0 |
| 31 | T1 | 17 | 6.3 | 0.415 | 9.3 | LOS A | 3.0 | 22.5 | 0.68 | 0.76 | 0.68 | 28.0 |
| 32 | R2 | 326 | 10.3 | 0.415 | 11.0 | LOS A | 3.0 | 22.5 | 0.68 | 0.76 | 0.68 | 50.3 |
| Approach |  | 944 | 7.5 | 0.574 | 8.5 | LOS A | 5.3 | 38.9 | 0.73 | 0.74 | 0.74 | 50.6 |
| All Ve | icles | 2817 | 6.3 | 0.768 | 11.0 | LOS A | 11.1 | 81.6 | 0.84 | 0.86 | 0.95 | 49.3 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## $\nabla$ Site: 101 [AM Ex Wallamore - Goddard]

Wallamore Road and Goddard Lane
Surveyed AM Peak
8:00am to 9:00am
Site Category: (None)
Giveway / Yield (Two-Way)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Deman <br> Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | $\begin{aligned} & \text { Deg. } \\ & \text { Satn } \\ & \text { v/c } \end{aligned}$ | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average <br> Speed km/h |
| SouthEast: Wallamore Road (SE) |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 | L2 | 123 | 20.5 | 0.076 | 7.9 | LOS A | 0.0 | 0.0 | 0.00 | 0.59 | 0.00 | 60.2 |
| 22 | T1 | 17 | 31.3 | 0.010 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 80.0 |
| Appr |  | 140 | 21.8 | 0.076 | 6.9 | NA | 0.0 | 0.0 | 0.00 | 0.52 | 0.00 | 62.0 |
| NorthWest: Wallamore Road (NW) |  |  |  |  |  |  |  |  |  |  |  |  |
| 28 | T1 | 43 | 17.1 | 0.025 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 80.0 |
| 29 | R2 | 8 | 12.5 | 0.007 | 7.5 | LOS A | 0.0 | 0.2 | 0.26 | 0.59 | 0.26 | 60.1 |
| Appr |  | 52 | 16.3 | 0.025 | 1.2 | NA | 0.0 | 0.2 | 0.04 | 0.10 | 0.04 | 75.9 |
| SouthWest: Goddard Lane |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 | L2 | 5 | 60.0 | 0.143 | 8.6 | LOS A | 0.6 | 4.8 | 0.26 | 0.63 | 0.26 | 50.7 |
| 32 | R2 | 116 | 16.4 | 0.143 | 8.3 | LOS A | 0.6 | 4.8 | 0.26 | 0.63 | 0.26 | 58.9 |
| Approach |  | 121 | 18.3 | 0.143 | 8.3 | LOS A | 0.6 | 4.8 | 0.26 | 0.63 | 0.26 | 58.5 |
| All Vehicles |  | 313 | 19.5 | 0.143 | 6.5 | NA | 0.6 | 4.8 | 0.11 | 0.49 | 0.11 | 62.4 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## $\nabla$ Site: 101 [PM Ex Goddard - Armstrong]

Goddard Lane and Armstrong Street
Surveyed PM Peak
$3: 15 \mathrm{pm}$ to $4: 15 \mathrm{pm}$
Site Category: (None)
Giveway / Yield (Two-Way)


Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

$\nabla$ Site: 101 [PM Ex Oxley - Baiada]
Surveyed PM Peak Hour
3.15 pm to 4.15 pm

Site Category: (None)
Giveway / Yield (Two-Way)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\underset{\text { ID }}{\text { Mov }}$ | Turn | Demand <br> Total veh/h | Flows HV $\%$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| 22 | T1 | 184 | 11.4 | 0.101 | 6.9 | LOS A | 0.0 | 0.0 | 0.00 | 0.65 | 0.00 | 72.1 |
| 23 | R2 | 4 | 100.0 | 0.004 | 8.8 | LOS A | 0.0 | 0.0 | 0.00 | 0.69 | 0.00 | 58.7 |
| Appr | ach | 188 | 13.4 | 0.101 | 7.0 | NA | 0.0 | 0.0 | 0.00 | 0.65 | 0.00 | 71.7 |
| NorthEast: Baiada Site Access |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 | L2 | 7 | 14.3 | 0.007 | 5.4 | LOS A | 0.0 | 0.2 | 0.30 | 0.52 | 0.30 | 52.9 |
| 26 | R2 | 1 | 0.0 | 0.007 | 6.7 | LOS A | 0.0 | 0.2 | 0.30 | 0.52 | 0.30 | 55.6 |
| Appr | ach | 8 | 12.5 | 0.007 | 5.5 | LOS A | 0.0 | 0.2 | 0.30 | 0.52 | 0.30 | 53.2 |
| NorthWest: Oxley Highway (NW) |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 | L2 | 1 | 0.0 | 0.111 | 7.8 | LOS A | 0.0 | 0.0 | 0.00 | 0.65 | 0.00 | 76.3 |
| 28 | T1 | 194 | 17.4 | 0.111 | 7.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.65 | 0.00 | 70.2 |
| Approach |  | 195 | 17.3 | 0.111 | 7.1 | NA | 0.0 | 0.0 | 0.00 | 0.65 | 0.00 | 70.2 |
| All Vehicles |  | 392 | 15.3 | 0.111 | 7.0 | NA | 0.0 | 0.2 | 0.01 | 0.65 | 0.01 | 70.5 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## $\theta$ Site: 101 [PM Ex Oxley - Duri]

Oxley Highway and Duri Road
Surveyed PM Peak
$3: 15 \mathrm{pm}$ to $4: 15 \mathrm{pm}$
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Deman <br> Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \text { \% } \end{aligned}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| NorthEast: Oxley Highway (NE) |  |  |  |  |  |  |  |  |  |  |  |  |
| 25 | T1 | 336 | 3.8 | 0.170 | 4.7 | LOS A | 0.0 | 0.0 | 0.00 | 0.46 | 0.00 | 55.5 |
| 26a | R1 | 340 | 6.8 | 0.300 | 9.2 | LOS A | 2.0 | 14.7 | 0.58 | 0.70 | 0.58 | 50.9 |
| Appr |  | 676 | 5.3 | 0.300 | 7.0 | LOS A | 2.0 | 14.7 | 0.29 | 0.58 | 0.29 | 53.1 |
| West: Oxley Highway (W) |  |  |  |  |  |  |  |  |  |  |  |  |
| 10a | L1 | 337 | 4.4 | 0.175 | 4.3 | LOS A | 0.0 | 0.0 | 0.00 | 0.47 | 0.00 | 55.5 |
| 12b | R3 | 340 | 8.7 | 0.279 | 10.5 | LOSA | 1.8 | 13.7 | 0.49 | 0.68 | 0.49 | 50.6 |
| Appr |  | 677 | 6.5 | 0.279 | 7.4 | LOS A | 1.8 | 13.7 | 0.25 | 0.57 | 0.25 | 52.9 |
| SouthWest: Duri Road |  |  |  |  |  |  |  |  |  |  |  |  |
| 30b | L3 | 244 | 11.2 | 0.156 | 4.2 | LOS A | 0.0 | 0.0 | 0.00 | 0.52 | 0.00 | 54.6 |
| 31 | T1 | 241 | 3.9 | 0.214 | 6.3 | LOS A | 1.3 | 9.7 | 0.55 | 0.60 | 0.55 | 53.2 |
| Approach |  | 485 | 7.6 | 0.214 | 5.2 | LOS A | 1.3 | 9.7 | 0.27 | 0.56 | 0.27 | 53.9 |
| All Vehicles |  | 1838 | 6.4 | 0.300 | 6.7 | LOS A | 2.0 | 14.7 | 0.27 | 0.57 | 0.27 | 53.2 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

[^6]
## MOVEMENT SUMMARY

## $\nabla$ Site: 101 [PM Ex Oxley - Goddard]

Oxley Hwy and Goddard Ln
Surveyed PM Peak
$3: 15 \mathrm{pm}$ to $4: 15 \mathrm{pm}$
Site Category: (None)
Giveway / Yield (Two-Way)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Demand Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| SouthEast: Oxley Highway (south-east) |  |  |  |  |  |  |  |  |  |  |  |  |
| 22 | T1 | 126 | 17.5 | 0.073 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 100.0 |
| 23 | R2 | 114 | 9.3 | 0.103 | 9.1 | LOS A | 0.4 | 3.2 | 0.34 | 0.65 | 0.34 | 65.0 |
| Appr |  | 240 | 13.6 | 0.103 | 4.3 | NA | 0.4 | 3.2 | 0.16 | 0.31 | 0.16 | 79.6 |
| NorthEast: Goddard Lane |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 | L2 | 147 | 5.7 | 0.244 | 8.4 | LOS A | 1.0 | 7.5 | 0.36 | 0.66 | 0.36 | 65.4 |
| 26 | R2 | 65 | 4.8 | 0.244 | 11.7 | LOS A | 1.0 | 7.5 | 0.36 | 0.66 | 0.36 | 65.0 |
| Appr |  | 213 | 5.4 | 0.244 | 9.4 | LOS A | 1.0 | 7.5 | 0.36 | 0.66 | 0.36 | 65.3 |
| NorthWest: Oxley Highway (north-west) |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 | L2 | 51 | 16.7 | 0.030 | 9.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.63 | 0.00 | 69.3 |
| 28 | T1 | 155 | 17.0 | 0.088 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 100.0 |
| Approach |  | 205 | 16.9 | 0.088 | 2.2 | NA | 0.0 | 0.0 | 0.00 | 0.15 | 0.00 | 90.0 |
| All Vehicles |  | 658 | 12.0 | 0.244 | 5.3 | NA | 1.0 | 7.5 | 0.18 | 0.37 | 0.18 | 76.9 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## Site: 101 [PM Ex Oxley - Marius - Brisbane]

Oxley Highway, Marius Street and Brisbane Street
Surveyed PM Peak Hour
3:00pm to $4: 00 \mathrm{pm}$
Site Category: (None)
Signals - Fixed Time Isolated Cycle Time $=114$ seconds (Site User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Demand <br> Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| SouthEast: Marius Street (SE) |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 | L2 | 80 | 34.2 | 0.080 | 13.0 | LOS A | 1.5 | 13.9 | 0.37 | 0.66 | 0.37 | 38.5 |
| 22 | T1 | 472 | 4.2 | 0.585 | 26.3 | LOS B | 19.8 | 143.3 | 0.81 | 0.72 | 0.81 | 39.6 |
| 23 | R2 | 66 | 6.3 | 0.217 | 34.9 | LOS C | 2.7 | 19.8 | 0.75 | 0.75 | 0.75 | 34.7 |
| Appr | ach | 618 | 8.3 | 0.585 | 25.5 | LOS B | 19.8 | 143.3 | 0.75 | 0.71 | 0.75 | 38.9 |
| NorthEast: Brisbane Street |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 | L2 | 85 | 1.2 | 0.421 | 46.4 | LOS D | 8.6 | 61.9 | 0.90 | 0.77 | 0.90 | 31.7 |
| 25 | T1 | 233 | 5.9 | 0.421 | 40.8 | LOS C | 8.6 | 62.8 | 0.90 | 0.76 | 0.90 | 30.3 |
| 26 | R2 | 40 | 2.6 | 0.421 | 46.4 | LOS D | 8.6 | 62.8 | 0.90 | 0.76 | 0.90 | 34.9 |
| Appr | ach | 358 | 4.4 | 0.421 | 42.8 | LOS D | 8.6 | 62.8 | 0.90 | 0.76 | 0.90 | 31.2 |
| NorthWest: Marius Street (NW) |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 | L2 | 58 | 9.1 | 0.323 | 28.4 | LOS B | 9.4 | 68.1 | 0.70 | 0.64 | 0.70 | 42.0 |
| 28 | T1 | 466 | 3.2 | 0.323 | 22.8 | LOS B | 9.6 | 69.3 | 0.70 | 0.62 | 0.70 | 41.2 |
| 29 | R2 | 62 | 0.0 | 0.272 | 44.3 | LOS D | 2.9 | 20.2 | 0.85 | 0.76 | 0.85 | 29.1 |
| Appr | ach | 586 | 3.4 | 0.323 | 25.6 | LOS B | 9.6 | 69.3 | 0.72 | 0.63 | 0.72 | 39.8 |
| SouthWest: Oxley Highway |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 | L2 | 56 | 0.0 | 0.163 | 48.0 | LOS D | 2.6 | 18.4 | 0.88 | 0.74 | 0.88 | 27.9 |
| 31 | T1 | 164 | 8.3 | 0.506 | 45.6 | LOS D | 8.3 | 62.4 | 0.94 | 0.77 | 0.94 | 29.3 |
| 32 | R2 | 234 | 8.1 | 0.723 | 55.3 | LOS D | 12.8 | 96.0 | 1.00 | 0.86 | 1.06 | 22.1 |
| Approach |  | 454 | 7.2 | 0.723 | 50.9 | LOS D | 12.8 | 96.0 | 0.96 | 0.81 | 1.00 | 25.4 |
| All V | icles | 2016 | 6.0 | 0.723 | 34.3 | LOS C | 19.8 | 143.3 | 0.82 | 0.72 | 0.82 | 34.3 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## $\theta$ Site: 101 [PM Ex Peel - Jewry]

Peel Street and Jewry Street
Surveyed PM Peak Hour
15:45am to 16:45am
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Turn | Deman <br> Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \text { \% } \end{aligned}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| SouthEast: Peel Street (SE) |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 | L2 | 300 | 8.1 | 0.568 | 14.3 | LOS A | 5.1 | 37.8 | 0.95 | 1.07 | 1.18 | 47.3 |
| 22 | T1 | 424 | 4.0 | 0.664 | 14.7 | LOS B | 7.5 | 54.0 | 1.00 | 1.11 | 1.33 | 48.3 |
| 23 | R2 | 9 | 0.0 | 0.664 | 18.5 | LOS B | 7.5 | 54.0 | 1.00 | 1.11 | 1.33 | 28.5 |
| Appr | ach | 734 | 5.6 | 0.664 | 14.6 | LOS B | 7.5 | 54.0 | 0.98 | 1.09 | 1.27 | 47.4 |
| NorthEast: Car Park |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 | L2 | 24 | 0.0 | 0.137 | 8.5 | LOS A | 0.6 | 4.5 | 0.80 | 0.80 | 0.80 | 27.4 |
| 25 | T1 | 17 | 0.0 | 0.137 | 8.5 | LOS A | 0.6 | 4.5 | 0.80 | 0.80 | 0.80 | 27.6 |
| 26 | R2 | 3 | 0.0 | 0.137 | 8.5 | LOS A | 0.6 | 4.5 | 0.80 | 0.80 | 0.80 | 27.7 |
| Appr | ach | 44 | 0.0 | 0.137 | 8.5 | LOS A | 0.6 | 4.5 | 0.80 | 0.80 | 0.80 | 27.5 |
| NorthWest: Peel Street (NW) |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 | L2 | 14 | 0.0 | 0.485 | 9.2 | LOS A | 3.7 | 26.9 | 0.79 | 0.82 | 0.83 | 28.3 |
| 28 | T1 | 347 | 3.3 | 0.485 | 8.9 | LOS A | 3.7 | 26.9 | 0.79 | 0.82 | 0.83 | 52.1 |
| 29 | R2 | 681 | 5.4 | 0.732 | 15.4 | LOS B | 9.7 | 70.8 | 0.95 | 0.97 | 1.21 | 47.6 |
| Appr | ach | 1042 | 4.6 | 0.732 | 13.2 | LOS A | 9.7 | 70.8 | 0.89 | 0.92 | 1.08 | 48.6 |
| SouthWest: Jewry Street |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 | L2 | 802 | 2.6 | 0.869 | 17.6 | LOS B | 17.4 | 124.4 | 1.00 | 1.17 | 1.61 | 45.4 |
| 31 | T1 | 19 | 5.6 | 0.591 | 12.8 | LOS A | 5.5 | 40.0 | 0.87 | 0.94 | 1.01 | 27.3 |
| 32 | R2 | 403 | 4.2 | 0.591 | 14.4 | LOS A | 5.5 | 40.0 | 0.87 | 0.94 | 1.01 | 48.3 |
| Approach |  | 1224 | 3.2 | 0.869 | 16.5 | LOS B | 17.4 | 124.4 | 0.95 | 1.09 | 1.41 | 45.9 |
| All V | icles | 3044 | 4.2 | 0.869 | 14.8 | LOS B | 17.4 | 124.4 | 0.94 | 1.03 | 1.25 | 46.7 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## $\nabla$ Site: 101 [PM Ex Wallamore - Goddard]

Wallamore Road and Goddard Lane
Surveyed PM Peak
3:30pm to 4:30pm
Site Category: (None)
Giveway / Yield (Two-Way)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Deman <br> Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| SouthEast: Wallamore Road (SE) |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 | L2 | 207 | 7.1 | 0.117 | 7.7 | LOS A | 0.0 | 0.0 | 0.00 | 0.60 | 0.00 | 64.0 |
| 22 | T1 | 43 | 14.6 | 0.024 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 80.0 |
| Appr |  | 251 | 8.4 | 0.117 | 6.4 | NA | 0.0 | 0.0 | 0.00 | 0.50 | 0.00 | 66.3 |
| NorthWest: Wallamore Road (NW) |  |  |  |  |  |  |  |  |  |  |  |  |
| 28 | T1 | 23 | 13.6 | 0.013 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 80.0 |
| 29 | R2 | 5 | 60.0 | 0.007 | 9.5 | LOS A | 0.0 | 0.3 | 0.39 | 0.62 | 0.39 | 47.9 |
| Appr |  | 28 | 22.2 | 0.013 | 1.8 | NA | 0.0 | 0.3 | 0.07 | 0.11 | 0.07 | 71.2 |
| SouthWest: Goddard Lane |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 | L2 | 12 | 0.0 | 0.275 | 7.8 | LOS A | 1.3 | 9.5 | 0.36 | 0.66 | 0.36 | 65.0 |
| 32 | R2 | 221 | 7.6 | 0.275 | 8.6 | LOS A | 1.3 | 9.5 | 0.36 | 0.66 | 0.36 | 61.0 |
| Approach |  | 233 | 7.2 | 0.275 | 8.6 | LOS A | 1.3 | 9.5 | 0.36 | 0.66 | 0.36 | 61.2 |
| All Vehicles |  | 512 | 8.6 | 0.275 | 7.1 | NA | 1.3 | 9.5 | 0.17 | 0.55 | 0.17 | 64.1 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## $\nabla$ site: 101 [AM PP Goddard - Armstrong]

Goddard Lane and Armstrong Street
AM Peak with Processing Plant
7:45am to 8:45am background +6 -7am plant traffic
Site Category: (None)
Giveway / Yield (Two-Way)

Movement Performance - Vehicles
Mov Turn
ID

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## $\theta$ Site: 101 [AM PP Oxley - Duri]

Oxley Highway and Duri Road
AM Peak with Processing Plant
8:00am to 9:00am background +6 -7am plant traffic
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Deman <br> Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| NorthEast: Oxley Highway (NE) |  |  |  |  |  |  |  |  |  |  |  |  |
| 25 | T1 | 160 | 5.9 | 0.082 | 4.7 | LOS A | 0.0 | 0.0 | 0.00 | 0.46 | 0.00 | 55.5 |
| 26a | R1 | 283 | 4.8 | 0.231 | 8.6 | LOS A | 1.5 | 10.8 | 0.48 | 0.65 | 0.48 | 51.3 |
| Appr |  | 443 | 5.2 | 0.231 | 7.2 | LOS A | 1.5 | 10.8 | 0.31 | 0.58 | 0.31 | 52.7 |
| West: Oxley Highway (W) |  |  |  |  |  |  |  |  |  |  |  |  |
| 10a | L1 | 280 | 5.3 | 0.147 | 4.3 | LOS A | 0.0 | 0.0 | 0.00 | 0.47 | 0.00 | 55.5 |
| 12b | R3 | 238 | 13.7 | 0.236 | 11.6 | LOS A | 1.5 | 11.8 | 0.62 | 0.74 | 0.62 | 50.0 |
| Appr |  | 518 | 9.1 | 0.236 | 7.6 | LOS A | 1.5 | 11.8 | 0.29 | 0.60 | 0.29 | 52.8 |
| SouthWest: Duri Road |  |  |  |  |  |  |  |  |  |  |  |  |
| 30b | L3 | 293 | 14.0 | 0.190 | 4.2 | LOS A | 0.0 | 0.0 | 0.00 | 0.52 | 0.00 | 54.5 |
| 31 | T1 | 435 | 3.6 | 0.362 | 6.2 | LOS A | 2.5 | 18.1 | 0.55 | 0.60 | 0.55 | 53.2 |
| Approach |  | 727 | 7.8 | 0.362 | 5.4 | LOS A | 2.5 | 18.1 | 0.33 | 0.57 | 0.33 | 53.7 |
| All Vehicles |  | 1688 | 7.5 | 0.362 | 6.5 | LOS A | 2.5 | 18.1 | 0.31 | 0.58 | 0.31 | 53.2 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## MOVEMENT SUMMARY

## $\nabla$ Site: 101 [AM PP Oxley - Goddard]

Oxley Hwy and Goddard Ln
AM Peak with Processing Plant
7:45am to 8:45am background +6 -7am plant traffic
Site Category: (None)
Giveway / Yield (Two-Way)

Movement Performance - Vehicles

| Mov TurnID | Demand Flows <br> Total HV veh/h \% |  | Deg. | Average Delay sec | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective Stop Rate | Aver. No. Average Cycles Speed km/h |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\begin{array}{r} \text { Satn } \\ \mathrm{v} / \mathrm{c} \end{array}$ |  |  | Vehicles veh | Distance m |  |  |  |  |
| SouthEast: Oxley Highway (south-east) 0 |  |  |  |  |  |  |  |  |  |  |  |
| 22 T1 | 122 | 22.4 | 0.072 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 100.0 |
| 23 R2 | 109 | 16.3 | 0.101 | 9.2 | LOS A | 0.4 | 3.3 | 0.33 | 0.64 | 0.33 | 62.7 |
| Approach | 232 | 19.5 | 0.101 | 4.4 | NA | 0.4 | 3.3 | 0.15 | 0.30 | 0.15 | 78.0 |
| NorthEast: Goddard Lane |  |  |  |  |  |  |  |  |  |  |  |
| 24 L2 | 65 | 43.5 | 0.156 | 8.8 | LOS A | 0.6 | 5.6 | 0.31 | 0.64 | 0.31 | 56.6 |
| 26 R2 | 48 | 23.9 | 0.156 | 11.9 | LOS A | 0.6 | 5.6 | 0.31 | 0.64 | 0.31 | 59.8 |
| Approach | 114 | 35.2 | 0.156 | 10.1 | LOS A | 0.6 | 5.6 | 0.31 | 0.64 | 0.31 | 57.9 |
| NorthWest: Oxley Highway (north-west) |  |  |  |  |  |  |  |  |  |  |  |
| 27 L2 | 87 | 9.6 | 0.050 | 8.9 | LOS A | 0.0 | 0.0 | 0.00 | 0.63 | 0.00 | 71.3 |
| 28 T1 | 100 | 18.9 | 0.058 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 100.0 |
| Approach | 187 | 14.6 | 0.058 | 4.2 | NA | 0.0 | 0.0 | 0.00 | 0.29 | 0.00 | 84.1 |
| All Vehicles | 533 | 21.1 | 0.156 | 5.5 | NA | 0.6 | 5.6 | 0.13 | 0.37 | 0.13 | 74.4 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## Site: 101 [AM PP Oxley - Marius - Brisbane]

Oxley Highway, Marius Street and Brisbane Street
AM Peak Hour with Processing Plant
8:15am to $9: 15 \mathrm{am}$ background $+6-7 \mathrm{am}$ plant traffic
Site Category: (None)
Signals - Fixed Time Isolated Cycle Time $=93$ seconds (Site User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Mov } \\ \text { ID } \end{gathered}$ | Turn | Demand <br> Total <br> veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| SouthEast: Marius Street (SE) |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 | L2 | 231 | 7.3 | 0.199 | 12.3 | LOS A | 4.1 | 30.3 | 0.42 | 0.69 | 0.42 | 41.4 |
| 22 | T1 | 443 | 6.4 | 0.688 | 28.4 | LOS B | 17.4 | 128.6 | 0.92 | 0.80 | 0.92 | 38.5 |
| 23 | R2 | 36 | 2.9 | 0.141 | 35.9 | LOS C | 1.3 | 9.4 | 0.81 | 0.73 | 0.81 | 34.4 |
| Appr | ach | 709 | 6.5 | 0.688 | 23.6 | LOS B | 17.4 | 128.6 | 0.75 | 0.76 | 0.75 | 38.9 |
| NorthEast: Brisbane Street |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 | L2 | 104 | 3.0 | 0.489 | 40.8 | LOS C | 7.8 | 57.4 | 0.93 | 0.79 | 0.93 | 33.5 |
| 25 | T1 | 242 | 7.8 | 0.489 | 35.2 | LOS C | 7.9 | 58.5 | 0.93 | 0.78 | 0.93 | 32.3 |
| 26 | R2 | 41 | 2.6 | 0.489 | 40.8 | LOS C | 7.9 | 58.5 | 0.93 | 0.77 | 0.93 | 36.9 |
| Appr | ach | 387 | 6.0 | 0.489 | 37.3 | LOS C | 7.9 | 58.5 | 0.93 | 0.78 | 0.93 | 33.3 |
| NorthWest: Marius Street (NW) |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 | L2 | 57 | 0.0 | 0.389 | 30.2 | LOS C | 8.4 | 62.5 | 0.80 | 0.70 | 0.80 | 41.3 |
| 28 | T1 | 434 | 10.0 | 0.389 | 24.8 | LOS B | 8.5 | 64.2 | 0.80 | 0.69 | 0.80 | 40.0 |
| 29 | R2 | 42 | 0.0 | 0.272 | 45.6 | LOS D | 1.8 | 12.6 | 0.92 | 0.75 | 0.92 | 28.7 |
| Appr |  | 533 | 8.1 | 0.389 | 27.1 | LOS B | 8.5 | 64.2 | 0.81 | 0.69 | 0.81 | 39.1 |
| SouthWest: Oxley Highway |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 | L2 | 43 | 2.4 | 0.096 | 34.7 | LOS C | 1.5 | 10.8 | 0.80 | 0.72 | 0.80 | 32.5 |
| 31 | T1 | 165 | 1.9 | 0.347 | 31.4 | LOS C | 6.2 | 44.5 | 0.87 | 0.71 | 0.87 | 34.8 |
| 32 | R2 | 195 | 11.9 | 0.460 | 38.3 | LOS C | 7.7 | 59.0 | 0.90 | 0.80 | 0.90 | 27.1 |
| Approach |  | 403 | 6.8 | 0.460 | 35.1 | LOS C | 7.7 | 59.0 | 0.88 | 0.76 | 0.88 | 30.9 |
| All V | icles | 2033 | 6.9 | 0.688 | 29.4 | LOS C | 17.4 | 128.6 | 0.83 | 0.75 | 0.83 | 36.2 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## $\theta$ Site: 101 [AM PP Peel - Jewry]

Peel Street and Jewry Street
AM Peak Hour with Processing Plant
8:15am to $9: 15 \mathrm{am}+6-7 \mathrm{am}$ plant traffic
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Turn | Deman <br> Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| SouthEast: Peel Street (SE) |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 | L2 | 320 | 9.5 | 0.527 | 12.3 | LOS A | 4.8 | 36.0 | 0.96 | 1.02 | 1.12 | 48.5 |
| 22 | T1 | 295 | 5.4 | 0.542 | 13.2 | LOS A | 4.8 | 35.1 | 0.96 | 1.05 | 1.15 | 49.2 |
| 23 | R2 | 4 | 0.0 | 0.542 | 16.9 | LOS B | 4.8 | 35.1 | 0.96 | 1.05 | 1.15 | 28.8 |
| Appr | ach | 619 | 7.5 | 0.542 | 12.8 | LOS A | 4.8 | 36.0 | 0.96 | 1.03 | 1.13 | 48.6 |
| NorthEast: Car Park |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 | L2 | 14 | 0.0 | 0.085 | 9.3 | LOS A | 0.4 | 2.8 | 0.81 | 0.81 | 0.81 | 27.2 |
| 25 | T1 | 9 | 0.0 | 0.085 | 9.3 | LOS A | 0.4 | 2.8 | 0.81 | 0.81 | 0.81 | 27.4 |
| 26 | R2 | 1 | 0.0 | 0.085 | 9.3 | LOS A | 0.4 | 2.8 | 0.81 | 0.81 | 0.81 | 27.6 |
| Appr | ach | 24 | 0.0 | 0.085 | 9.3 | LOS A | 0.4 | 2.8 | 0.81 | 0.81 | 0.81 | 27.3 |
| NorthWest: Peel Street (NW) |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 | L2 | 13 | 8.3 | 0.540 | 9.2 | LOS A | 4.5 | 32.4 | 0.76 | 0.79 | 0.82 | 28.3 |
| 28 | T1 | 525 | 3.8 | 0.774 | 9.1 | LOS A | 11.4 | 83.6 | 0.79 | 0.81 | 0.88 | 51.6 |
| 29 | R2 | 713 | 5.6 | 0.774 | 15.2 | LOS B | 11.4 | 83.6 | 0.94 | 0.93 | 1.19 | 48.0 |
| Appr | ach | 1251 | 4.9 | 0.774 | 12.5 | LOS A | 11.4 | 83.6 | 0.87 | 0.88 | 1.06 | 49.1 |
| SouthWest: Jewry Street |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 | L2 | 602 | 5.9 | 0.576 | 7.1 | LOS A | 5.3 | 39.2 | 0.76 | 0.73 | 0.78 | 52.0 |
| 31 | T1 | 17 | 6.3 | 0.417 | 9.3 | LOS A | 3.0 | 22.6 | 0.68 | 0.76 | 0.68 | 28.0 |
| 32 | R2 | 327 | 10.3 | 0.417 | 11.0 | LOS A | 3.0 | 22.6 | 0.68 | 0.76 | 0.68 | 50.3 |
| Approach |  | 946 | 7.5 | 0.576 | 8.5 | LOS A | 5.3 | 39.2 | 0.73 | 0.74 | 0.74 | 50.6 |
| All V | icles | 2840 | 6.3 | 0.774 | 11.2 | LOS A | 11.4 | 83.6 | 0.84 | 0.87 | 0.97 | 49.2 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## $\nabla$ Site: 101 [AM PP Wallamore - Goddard]

Wallamore Road and Goddard Lane
AM Peak with Processing Plant
8:00am to 9:00am background +6 -7am plant traffic
Site Category: (None)
Giveway / Yield (Two-Way)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | Demand Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| SouthEast: Wallamore Road (SE) |  |  |  |  |  |  |  |  |  |  |  |
| 21 L2 | 153 | 16.6 | 0.092 | 7.8 | LOS A | 0.0 | 0.0 | 0.00 | 0.59 | 0.00 | 61.3 |
| 22 T1 | 17 | 31.3 | 0.010 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 80.0 |
| Approach | 169 | 18.0 | 0.092 | 7.0 | NA | 0.0 | 0.0 | 0.00 | 0.53 | 0.00 | 62.7 |
| NorthWest: Wallamore Road (NW) |  |  |  |  |  |  |  |  |  |  |  |
| 28 T1 | 43 | 17.1 | 0.025 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 80.0 |
| 29 R2 | 9 | 11.1 | 0.008 | 7.6 | LOS A | 0.0 | 0.2 | 0.29 | 0.59 | 0.29 | 60.4 |
| Approach | 53 | 16.0 | 0.025 | 1.4 | NA | 0.0 | 0.2 | 0.05 | 0.11 | 0.05 | 75.6 |
| SouthWest: Goddard Lane |  |  |  |  |  |  |  |  |  |  |  |
| 30 L2 | 5 | 60.0 | 0.150 | 8.6 | LOS A | 0.6 | 5.1 | 0.27 | 0.63 | 0.27 | 50.6 |
| 32 R2 | 119 | 15.9 | 0.150 | 8.4 | LOS A | 0.6 | 5.1 | 0.27 | 0.63 | 0.27 | 58.9 |
| Approach | 124 | 17.8 | 0.150 | 8.4 | LOS A | 0.6 | 5.1 | 0.27 | 0.63 | 0.27 | 58.5 |
| All Vehicles | 346 | 17.6 | 0.150 | 6.7 | NA | 0.6 | 5.1 | 0.11 | 0.51 | 0.11 | 62.7 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## $\nabla$ Site: 101 [PM PP Goddard - Armstrong]

Goddard Lane and Armstrong Street
PM Peak with Processing Plant
$3: 15 \mathrm{pm}$ to $4: 15 \mathrm{pm}$ background $+3-4 \mathrm{pm}$ plant traffic
Site Category: (None)
Giveway / Yield (Two-Way)

Movement Performance - Vehicles

| Mov | Turn | Demand | Fows | Deg. | Average | Level of | 95\% Back | of Queue | Prop. | Effective | Aver. No. | Average |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ID |  | Total veh/h | $\begin{array}{r} \mathrm{HV} \\ \% \end{array}$ | Satn v/c | Delay sec | Service | Vehicles veh | Distance m | Queued | Stop Rate | Cycles | Speed km/h |
| Nort | st: G | dard Lan | north |  |  |  |  |  |  |  |  |  |
| 25 | T1 | 139 | 4.5 | 0.087 | 0.1 | LOS A | 0.1 | 1.0 | 0.08 | 0.06 | 0.08 | 78.0 |
| 26 | R2 | 14 | 46.2 | 0.087 | 8.5 | LOS A | 0.1 | 1.0 | 0.08 | 0.06 | 0.08 | 58.2 |
| Approad |  | 153 | 8.3 | 0.087 | 0.9 | NA | 0.1 | 1.0 | 0.08 | 0.06 | 0.08 | 74.5 |
| North | est: A | trong St |  |  |  |  |  |  |  |  |  |  |
| 27 | L2 | 105 | 7.0 | 0.300 | 4.9 | LOS A | 1.3 | 9.5 | 0.25 | 0.58 | 0.25 | 51.7 |
| 29 | R2 | 216 | 8.8 | 0.300 | 6.2 | LOS A | 1.3 | 9.5 | 0.25 | 0.58 | 0.25 | 33.4 |
| Appr |  | 321 | 8.2 | 0.300 | 5.8 | LOS A | 1.3 | 9.5 | 0.25 | 0.58 | 0.25 | 39.6 |
| South | est: | dard Lan | sout | est) |  |  |  |  |  |  |  |  |
| 30 | L2 | 112 | 17.9 | 0.105 | 5.7 | LOS A | 0.0 | 0.0 | 0.00 | 0.39 | 0.00 | 55.8 |
| 31 | T1 | 65 | 19.4 | 0.105 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.39 | 0.00 | 70.9 |
| Appr |  | 177 | 18.5 | 0.105 | 3.6 | NA | 0.0 | 0.0 | 0.00 | 0.39 | 0.00 | 60.6 |
| All Ve | icles | 651 | 11.0 | 0.300 | 4.0 | NA | 1.3 | 9.5 | 0.14 | 0.41 | 0.14 | 48.8 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## $\theta$ Site: 101 [PM PP Oxley - Duri]

Oxley Highway and Duri Road
PM Peak with Processing Plant
$3: 15 \mathrm{pm}$ to $4: 15 \mathrm{pm}$ background $+3-4 \mathrm{pm}$ plant traffic
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Deman <br> Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| NorthEast: Oxley Highway (NE) |  |  |  |  |  |  |  |  |  |  |  |  |
| 25 | T1 | 336 | 3.8 | 0.170 | 4.7 | LOS A | 0.0 | 0.0 | 0.00 | 0.46 | 0.00 | 55.5 |
| 26a | R1 | 342 | 7.4 | 0.319 | 9.6 | LOS A | 2.2 | 16.0 | 0.63 | 0.73 | 0.63 | 50.8 |
| Appr |  | 678 | 5.6 | 0.319 | 7.2 | LOS A | 2.2 | 16.0 | 0.32 | 0.60 | 0.32 | 53.0 |
| West: Oxley Highway (W) |  |  |  |  |  |  |  |  |  |  |  |  |
| 10a | L1 | 395 | 4.0 | 0.205 | 4.3 | LOS A | 0.0 | 0.0 | 0.00 | 0.47 | 0.00 | 55.5 |
| 12b | R3 | 401 | 8.4 | 0.327 | 10.5 | LOSA | 2.2 | 16.8 | 0.51 | 0.68 | 0.51 | 50.5 |
| Appr |  | 796 | 6.2 | 0.327 | 7.4 | LOS A | 2.2 | 16.8 | 0.26 | 0.58 | 0.26 | 52.9 |
| SouthWest: Duri Road |  |  |  |  |  |  |  |  |  |  |  |  |
| 30b | L3 | 249 | 13.1 | 0.161 | 4.2 | LOS A | 0.0 | 0.0 | 0.00 | 0.52 | 0.00 | 54.5 |
| 31 | T1 | 241 | 3.9 | 0.215 | 6.3 | LOS A | 1.4 | 9.9 | 0.56 | 0.61 | 0.56 | 53.2 |
| Approach |  | 491 | 8.6 | 0.215 | 5.2 | LOS A | 1.4 | 9.9 | 0.27 | 0.56 | 0.27 | 53.8 |
| All Vehicles |  | 1964 | 6.6 | 0.327 | 6.8 | LOS A | 2.2 | 16.8 | 0.28 | 0.58 | 0.28 | 53.2 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## MOVEMENT SUMMARY

## $\nabla$ Site: 101 [PM PP Oxley - Goddard]

Oxley Hwy and Goddard Ln
PM Peak with Processing Plant
$3: 15 \mathrm{pm}$ to $4: 15 \mathrm{pm}$ background $+3-4 \mathrm{pm}$ plant traffic
Site Category: (None)
Giveway / Yield (Two-Way)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{ll} \text { Mov Turn } \\ \text { ID } \end{array}$ | Deman <br> Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| SouthEast: Oxley Highway (south-east) |  |  |  |  |  |  |  |  |  |  |  |
| 22 T1 | 124 | 16.1 | 0.071 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 100.0 |
| 23 R2 | 122 | 15.5 | 0.115 | 9.3 | LOS A | 0.5 | 3.8 | 0.35 | 0.65 | 0.35 | 62.9 |
| Approach | 246 | 15.8 | 0.115 | 4.6 | NA | 0.5 | 3.8 | 0.17 | 0.32 | 0.17 | 77.3 |
| NorthEast: Goddard Lane |  |  |  |  |  |  |  |  |  |  |  |
| 24 L2 | 274 | 6.2 | 0.381 | 8.6 | LOS A | 1.9 | 14.2 | 0.38 | 0.66 | 0.40 | 65.1 |
| 26 R2 | 76 | 9.7 | 0.381 | 13.1 | LOSA | 1.9 | 14.2 | 0.38 | 0.66 | 0.40 | 63.5 |
| Approach | 349 | 6.9 | 0.381 | 9.6 | LOS A | 1.9 | 14.2 | 0.38 | 0.66 | 0.40 | 64.8 |
| NorthWest: Oxley Highway (north-west) |  |  |  |  |  |  |  |  |  |  |  |
| 27 L2 | 55 | 23.1 | 0.034 | 9.2 | LOS A | 0.0 | 0.0 | 0.00 | 0.63 | 0.00 | 67.5 |
| 28 T1 | 148 | 17.0 | 0.085 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 100.0 |
| Approach | 203 | 18.7 | 0.085 | 2.5 | NA | 0.0 | 0.0 | 0.00 | 0.17 | 0.00 | 88.4 |
| All Vehicles | 799 | 12.6 | 0.381 | 6.3 | NA | 1.9 | 14.2 | 0.22 | 0.43 | 0.23 | 73.4 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## Site: 101 [PM PP Oxley - Marius - Brisbane]

Oxley Highway, Marius Street and Brisbane Street
PM Peak Hour with Processing Plant
3:00pm to $4: 00 \mathrm{pm}$ background $+3-4 \mathrm{pm}$ plant traffic
Site Category: (None)
Signals - Fixed Time Isolated Cycle Time $=114$ seconds (Site User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Mov } \\ \text { ID } \end{gathered}$ | Turn | Deman <br> Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| SouthEast: Marius Street (SE) |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 | L2 | 293 | 10.4 | 0.254 | 13.7 | LOS A | 6.4 | 48.8 | 0.43 | 0.70 | 0.43 | 40.0 |
| 22 | T1 | 452 | 4.4 | 0.554 | 26.0 | LOS B | 18.7 | 135.6 | 0.80 | 0.71 | 0.80 | 39.7 |
| 23 | R2 | 65 | 6.5 | 0.213 | 34.9 | LOS C | 2.6 | 19.4 | 0.75 | 0.75 | 0.75 | 34.8 |
| Appr | ach | 809 | 6.8 | 0.554 | 22.3 | LOS B | 18.7 | 135.6 | 0.66 | 0.71 | 0.66 | 39.3 |
| NorthEast: Brisbane Street |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 | L2 | 85 | 1.2 | 0.421 | 46.4 | LOS D | 8.6 | 61.9 | 0.90 | 0.77 | 0.90 | 31.7 |
| 25 | T1 | 233 | 5.9 | 0.421 | 40.8 | LOS C | 8.6 | 62.8 | 0.90 | 0.76 | 0.90 | 30.3 |
| 26 | R2 | 40 | 2.6 | 0.421 | 46.4 | LOS D | 8.6 | 62.8 | 0.90 | 0.76 | 0.90 | 34.9 |
| Appr | ach | 358 | 4.4 | 0.421 | 42.8 | LOS D | 8.6 | 62.8 | 0.90 | 0.76 | 0.90 | 31.2 |
| NorthWest: Marius Street (NW) |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 | L2 | 58 | 9.1 | 0.323 | 28.4 | LOS B | 9.4 | 68.1 | 0.70 | 0.64 | 0.70 | 42.0 |
| 28 | T1 | 466 | 3.2 | 0.323 | 22.8 | LOS B | 9.6 | 69.3 | 0.70 | 0.62 | 0.70 | 41.2 |
| 29 | R2 | 62 | 0.0 | 0.308 | 44.2 | LOS D | 2.9 | 20.4 | 0.85 | 0.77 | 0.85 | 29.2 |
| Appr |  | 586 | 3.4 | 0.323 | 25.6 | LOS B | 9.6 | 69.3 | 0.72 | 0.63 | 0.72 | 39.8 |
| SouthWest: Oxley Highway |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 | L2 | 64 | 0.0 | 0.188 | 48.2 | LOS D | 3.0 | 21.3 | 0.88 | 0.75 | 0.88 | 27.8 |
| 31 | T1 | 180 | 7.6 | 0.568 | 46.0 | LOS D | 9.2 | 68.7 | 0.95 | 0.78 | 0.95 | 29.1 |
| 32 | R2 | 251 | 8.0 | 0.774 | 57.4 | LOS E | 14.2 | 106.2 | 1.00 | 0.89 | 1.12 | 21.6 |
| Approach |  | 495 | 6.8 | 0.774 | 52.1 | LOS D | 14.2 | 106.2 | 0.97 | 0.83 | 1.03 | 25.1 |
| All V | icles | 2248 | 5.5 | 0.774 | 33.0 | LOS C | 18.7 | 135.6 | 0.78 | 0.73 | 0.80 | 34.3 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## $\theta$ Site: 101 [PM PP Peel - Jewry]

Peel Street and Jewry Street
PM Peak Hour with Processing Plant
15:45am to 16:45am background $+3-4 \mathrm{pm}$ plant traffic
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Turn | Deman <br> Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \text { \% } \end{aligned}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| SouthEast: Peel Street (SE) |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 | L2 | 300 | 8.1 | 0.574 | 14.4 | LOS A | 5.2 | 38.7 | 0.96 | 1.07 | 1.19 | 47.2 |
| 22 | T1 | 424 | 4.0 | 0.672 | 15.0 | LOS B | 7.7 | 55.3 | 1.00 | 1.12 | 1.34 | 48.1 |
| 23 | R2 | 9 | 0.0 | 0.672 | 18.8 | LOS B | 7.7 | 55.3 | 1.00 | 1.12 | 1.34 | 28.4 |
| Appr | ach | 734 | 5.6 | 0.672 | 14.8 | LOS B | 7.7 | 55.3 | 0.98 | 1.10 | 1.28 | 47.3 |
| NorthEast: Car Park |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 | L2 | 24 | 0.0 | 0.143 | 9.0 | LOS A | 0.7 | 4.7 | 0.81 | 0.81 | 0.81 | 27.3 |
| 25 | T1 | 17 | 0.0 | 0.143 | 9.0 | LOS A | 0.7 | 4.7 | 0.81 | 0.81 | 0.81 | 27.5 |
| 26 | R2 | 3 | 0.0 | 0.143 | 9.0 | LOS A | 0.7 | 4.7 | 0.81 | 0.81 | 0.81 | 27.6 |
| Appr | ach | 44 | 0.0 | 0.143 | 9.0 | LOS A | 0.7 | 4.7 | 0.81 | 0.81 | 0.81 | 27.4 |
| NorthWest: Peel Street (NW) |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 | L2 | 14 | 0.0 | 0.505 | 9.8 | LOS A | 4.1 | 29.2 | 0.82 | 0.87 | 0.89 | 28.1 |
| 28 | T1 | 347 | 3.3 | 0.505 | 9.6 | LOS A | 4.1 | 29.2 | 0.82 | 0.87 | 0.89 | 51.6 |
| 29 | R2 | 681 | 5.4 | 0.762 | 16.9 | LOS B | 10.8 | 79.1 | 0.99 | 1.03 | 1.33 | 46.7 |
| Appr | ach | 1042 | 4.6 | 0.762 | 14.4 | LOS A | 10.8 | 79.1 | 0.93 | 0.98 | 1.18 | 47.8 |
| SouthWest: Jewry Street |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 | L2 | 824 | 2.6 | 0.891 | 19.6 | LOS B | 19.6 | 140.2 | 1.00 | 1.23 | 1.73 | 44.4 |
| 31 | T1 | 19 | 5.6 | 0.627 | 13.4 | LOS A | 6.3 | 45.5 | 0.89 | 0.96 | 1.07 | 27.2 |
| 32 | R2 | 437 | 3.9 | 0.627 | 14.9 | LOS B | 6.3 | 45.5 | 0.89 | 0.96 | 1.07 | 48.0 |
| Approach |  | 1280 | 3.0 | 0.891 | 17.9 | LOS B | 19.6 | 140.2 | 0.96 | 1.13 | 1.49 | 45.1 |
| All V | icles | 3100 | 4.1 | 0.891 | 15.9 | LOS B | 19.6 | 140.2 | 0.95 | 1.07 | 1.33 | 46.1 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## $\nabla$ Site: 101 [PM PP Wallamore - Goddard]

Wallamore Road and Goddard Lane
PM Peak with Processing Plant
3:30pm to $4: 30 \mathrm{pm}$ background $+3-4 \mathrm{pm}$ plant traffic
Site Category: (None)
Giveway / Yield (Two-Way)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Deman <br> Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | $\begin{aligned} & \text { Deg. } \\ & \text { Satn } \\ & \text { v/c } \end{aligned}$ | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average <br> Speed km/h |
| SouthEast: Wallamore Road (SE) |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 | L2 | 207 | 7.1 | 0.117 | 7.7 | LOS A | 0.0 | 0.0 | 0.00 | 0.60 | 0.00 | 64.0 |
| 22 | T1 | 43 | 14.6 | 0.024 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 80.0 |
| Appr |  | 251 | 8.4 | 0.117 | 6.4 | NA | 0.0 | 0.0 | 0.00 | 0.50 | 0.00 | 66.3 |
| NorthWest: Wallamore Road (NW) |  |  |  |  |  |  |  |  |  |  |  |  |
| 28 | T1 | 23 | 13.6 | 0.013 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 80.0 |
| 29 | R2 | 5 | 60.0 | 0.007 | 9.5 | LOS A | 0.0 | 0.3 | 0.39 | 0.62 | 0.39 | 47.9 |
| Appr |  | 28 | 22.2 | 0.013 | 1.8 | NA | 0.0 | 0.3 | 0.07 | 0.11 | 0.07 | 71.2 |
| SouthWest: Goddard Lane |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 | L2 | 16 | 0.0 | 0.368 | 7.8 | LOS A | 1.9 | 13.7 | 0.39 | 0.66 | 0.39 | 64.8 |
| 32 | R2 | 300 | 5.6 | 0.368 | 8.8 | LOS A | 1.9 | 13.7 | 0.39 | 0.66 | 0.39 | 61.5 |
| Approach |  | 316 | 5.3 | 0.368 | 8.7 | LOS A | 1.9 | 13.7 | 0.39 | 0.66 | 0.39 | 61.6 |
| All Vehicles |  | 595 | 7.4 | 0.368 | 7.4 | NA | 1.9 | 13.7 | 0.21 | 0.57 | 0.21 | 63.9 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## $\nabla$ Site: 101 [AM Growth Goddard - Armstrong]

Goddard Lane and Armstrong Street
AM Peak with Growth
7:45am to 8:45am background + growth
Site Category: (None)
Giveway / Yield (Two-Way)

Movement Performance - Vehicles

| MovID | Turn | Demand | Flows | Deg. | Average | Level of | 95\% Back | of Queue | Prop. | Effective | Aver. No. | Average |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Total veh/h | $\begin{array}{r} \text { HV } \\ \% \end{array}$ | Satn v/c | Delay sec | Service | Vehicles veh | Distance m | Queued | Stop Rate | Cycles | Speed km/h |
| NorthEast: Goddard Lane (north-east) |  |  |  |  |  |  |  |  |  |  |  |  |
| 25 | T1 | 81 | 22.1 | 0.069 | 0.3 | LOS A | 0.2 | 1.7 | 0.16 | 0.14 | 0.16 | 74.6 |
| 26 | R2 | 24 | 39.1 | 0.069 | 8.2 | LOS A | 0.2 | 1.7 | 0.16 | 0.14 | 0.16 | 57.3 |
| Appr | ach | 105 | 26.0 | 0.069 | 2.1 | NA | 0.2 | 1.7 | 0.16 | 0.14 | 0.16 | 67.9 |
| NorthWest: Armstrong Street |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 | L2 | 13 | 50.0 | 0.059 | 5.6 | LOS A | 0.2 | 2.0 | 0.30 | 0.58 | 0.30 | 43.8 |
| 29 | R2 | 38 | 44.4 | 0.059 | 6.5 | LOS A | 0.2 | 2.0 | 0.30 | 0.58 | 0.30 | 32.4 |
| Approach |  | 51 | 45.8 | 0.059 | 6.3 | LOS A | 0.2 | 2.0 | 0.30 | 0.58 | 0.30 | 35.6 |
| SouthWest: Goddard Lane (south-west) |  |  |  |  |  |  |  |  |  |  |  |  |
| $\begin{aligned} & 30 \\ & 31 \end{aligned}$ | L2 | 52 | 22.4 | 0.094 | 5.7 | LOS A | 0.0 | 0.0 | 0.00 | 0.19 | 0.00 | 56.8 |
|  | T1 | 117 | 5.4 | 0.094 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.19 | 0.00 | 75.9 |
| Approach |  | 168 | 10.6 | 0.094 | 1.7 | NA | 0.0 | 0.0 | 0.00 | 0.19 | 0.00 | 68.8 |
| All Vehicles |  | 324 | 21.1 | 0.094 | 2.6 | NA | 0.2 | 2.0 | 0.10 | 0.24 | 0.10 | 59.2 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## $\theta$ Site: 101 [AM Growth Oxley - Duri]

Oxley Highway and Duri Road
AM Peak with Growth
8:00am to 9:00am background + growth
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Mov } \\ \text { ID } \end{gathered}$ | Turn | Deman <br> Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| NorthEast: Oxley Highway (NE) |  |  |  |  |  |  |  |  |  |  |  |  |
| 25 | T1 | 193 | 6.0 | 0.099 | 4.7 | LOS A | 0.0 | 0.0 | 0.00 | 0.46 | 0.00 | 55.5 |
| 26a | R1 | 313 | 4.4 | 0.266 | 8.8 | LOS A | 1.8 | 12.9 | 0.54 | 0.67 | 0.54 | 51.1 |
| Appr | ach | 505 | 5.0 | 0.266 | 7.2 | LOS A | 1.8 | 12.9 | 0.33 | 0.59 | 0.33 | 52.7 |
| West: Oxley Highway (W) |  |  |  |  |  |  |  |  |  |  |  |  |
| 10a | L1 | 332 | 4.8 | 0.173 | 4.3 | LOS A | 0.0 | 0.0 | 0.00 | 0.47 | 0.00 | 55.5 |
| 12b | R3 | 279 | 12.5 | 0.300 | 12.2 | LOSA | 2.1 | 16.0 | 0.71 | 0.79 | 0.71 | 49.8 |
| Appr | ach | 611 | 8.3 | 0.300 | 7.9 | LOS A | 2.1 | 16.0 | 0.33 | 0.62 | 0.33 | 52.7 |
| SouthWest: Duri Road |  |  |  |  |  |  |  |  |  |  |  |  |
| 30b | L3 | 322 | 13.7 | 0.208 | 4.2 | LOS A | 0.0 | 0.0 | 0.00 | 0.52 | 0.00 | 54.5 |
| 31 | T1 | 522 | 3.6 | 0.446 | 6.5 | LOSA | 3.4 | 24.3 | 0.63 | 0.64 | 0.63 | 52.9 |
| Approach |  | 844 | 7.5 | 0.446 | 5.6 | LOS A | 3.4 | 24.3 | 0.39 | 0.60 | 0.39 | 53.5 |
| All Vehicles |  | 1960 | 7.1 | 0.446 | 6.8 | LOS A | 3.4 | 24.3 | 0.35 | 0.60 | 0.35 | 53.0 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## $\nabla$ Site: 101 [AM Growth Oxley - Goddard]

Oxley Hwy and Goddard Ln
AM Peak with Growth
7:45am to 8:45am background + growth
Site Category: (None)
Giveway / Yield (Two-Way)


Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## Site: 101 [AM Growth Oxley - Marius - Brisbane]

Oxley Highway, Marius Street and Brisbane Street
AM Peak Hour with Growth
8:15am to 9:15am background + growth
Site Category: (None)
Signals - Fixed Time Isolated Cycle Time $=93$ seconds (Site User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Turn | Demand <br> Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| SouthEast: Marius Street (SE) |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 | L2 | 267 | 6.3 | 0.229 | 12.5 | LOS A | 4.8 | 35.7 | 0.43 | 0.70 | 0.43 | 41.4 |
| 22 | T1 | 533 | 6.5 | 0.862 | 38.9 | LOS C | 25.9 | 191.4 | 0.98 | 1.01 | 1.18 | 34.0 |
| 23 | R2 | 44 | 4.8 | 0.206 | 38.5 | LOS C | 1.7 | 12.4 | 0.85 | 0.74 | 0.85 | 33.4 |
| Appr |  | 844 | 6.4 | 0.862 | 30.5 | LOS C | 25.9 | 191.4 | 0.80 | 0.90 | 0.92 | 35.4 |
| NorthEast: Brisbane Street |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 | L2 | 126 | 3.3 | 0.585 | 41.7 | LOS C | 9.6 | 70.4 | 0.95 | 0.81 | 0.95 | 33.2 |
| 25 | T1 | 285 | 8.1 | 0.585 | 36.1 | LOS C | 9.7 | 71.8 | 0.95 | 0.80 | 0.95 | 32.0 |
| 26 | R2 | 51 | 4.2 | 0.585 | 41.7 | LOS C | 9.7 | 71.8 | 0.95 | 0.80 | 0.95 | 36.6 |
| Appr | ach | 462 | 6.4 | 0.585 | 38.2 | LOS C | 9.7 | 71.8 | 0.95 | 0.80 | 0.95 | 32.9 |
| NorthWest: Marius Street (NW) |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 | L2 | 68 | 0.0 | 0.489 | 31.2 | LOS C | 11.0 | 81.9 | 0.83 | 0.73 | 0.83 | 40.8 |
| 28 | T1 | 522 | 10.1 | 0.489 | 25.6 | LOS B | 11.0 | 81.9 | 0.83 | 0.71 | 0.83 | 39.6 |
| 29 | R2 | 47 | 0.0 | 0.422 | 52.7 | LOS D | 2.2 | 15.5 | 0.99 | 0.75 | 0.99 | 26.6 |
| Appr |  | 638 | 8.3 | 0.489 | 28.2 | LOS B | 11.0 | 81.9 | 0.84 | 0.72 | 0.84 | 38.6 |
| SouthWest: Oxley Highway |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 | L2 | 53 | 4.0 | 0.118 | 35.0 | LOS C | 1.9 | 13.5 | 0.81 | 0.73 | 0.81 | 32.4 |
| 31 | T1 | 199 | 2.1 | 0.421 | 32.1 | LOS C | 7.7 | 54.7 | 0.89 | 0.73 | 0.89 | 34.5 |
| 32 | R2 | 232 | 10.9 | 0.543 | 39.1 | LOS C | 9.3 | 71.4 | 0.92 | 0.82 | 0.92 | 26.9 |
| Approach |  | 483 | 6.5 | 0.543 | 35.8 | LOS C | 9.3 | 71.4 | 0.90 | 0.77 | 0.90 | 30.7 |
| All V | icles | 2427 | 6.9 | 0.862 | 32.4 | LOS C | 25.9 | 191.4 | 0.86 | 0.81 | 0.90 | 34.8 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## 9 Site: 101 [AM Growth Peel - Jewry]

Peel Street and Jewry Street
AM Peak Hour with Growth
8:15am to 9:15am + growth
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Turn | Demand <br> Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| SouthEast: Peel Street (SE) |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 | L2 | 369 | 10.0 | 0.768 | 25.5 | LOS B | 9.8 | 74.3 | 1.00 | 1.25 | 1.64 | 41.3 |
| 22 | T1 | 354 | 5.4 | 0.828 | 32.8 | LOS C | 11.4 | 83.2 | 1.00 | 1.33 | 1.88 | 39.0 |
| 23 | R2 | 5 | 0.0 | 0.828 | 36.5 | LOS C | 11.4 | 83.2 | 1.00 | 1.33 | 1.88 | 25.0 |
| Appr | ach | 728 | 7.7 | 0.828 | 29.1 | LOS C | 11.4 | 83.2 | 1.00 | 1.29 | 1.76 | 40.0 |
| NorthEast: Car Park |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 | L2 | 17 | 0.0 | 0.152 | 14.9 | LOS B | 0.7 | 5.2 | 0.88 | 0.88 | 0.88 | 26.2 |
| 25 | T1 | 12 | 0.0 | 0.152 | 14.9 | LOS B | 0.7 | 5.2 | 0.88 | 0.88 | 0.88 | 26.3 |
| 26 | R2 | 1 | 0.0 | 0.152 | 14.9 | LOS B | 0.7 | 5.2 | 0.88 | 0.88 | 0.88 | 26.5 |
| Appr |  | 29 | 0.0 | 0.152 | 14.9 | LOS B | 0.7 | 5.2 | 0.88 | 0.88 | 0.88 | 26.2 |
| NorthWest: Peel Street (NW) |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 | L2 | 17 | 12.5 | 0.704 | 13.7 | LOS A | 8.2 | 59.3 | 0.92 | 1.01 | 1.20 | 27.5 |
| 28 | T1 | 631 | 3.8 | 1.009 | 19.7 | LOS B | 46.4 | 340.2 | 0.94 | 1.17 | 1.59 | 44.9 |
| 29 | R2 | 846 | 5.7 | 1.009 | 54.6 | LOS D | 46.4 | 340.2 | 1.00 | 1.90 | 3.39 | 31.8 |
| Appr |  | 1494 | 5.0 | 1.009 | 39.4 | LOS C | 46.4 | 340.2 | 0.97 | 1.58 | 2.61 | 36.2 |
| SouthWest: Jewry Street |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 | L2 | 722 | 6.0 | 0.737 | 10.5 | LOS A | 9.9 | 73.2 | 0.94 | 0.91 | 1.14 | 49.8 |
| 31 | T1 | 21 | 10.0 | 0.539 | 11.1 | LOS A | 4.6 | 35.0 | 0.79 | 0.85 | 0.86 | 27.7 |
| 32 | R2 | 393 | 10.5 | 0.539 | 12.7 | LOS A | 4.6 | 35.0 | 0.79 | 0.85 | 0.86 | 49.3 |
| Approach |  | 1136 | 7.6 | 0.737 | 11.3 | LOS A | 9.9 | 73.2 | 0.88 | 0.89 | 1.04 | 48.9 |
| All V | icles | 3387 | 6.4 | 1.009 | 27.5 | LOS B | 46.4 | 340.2 | 0.95 | 1.28 | 1.88 | 40.4 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

$\nabla$ site: 101 [AM Growth Wallamore - Goddard]
Wallamore Road and Goddard Lane
AM Peak with Growth
8:00am to 9:00am background + growth
Site Category: (None)
Giveway / Yield (Two-Way)

Movement Performance - Vehicles

| Mov ID | Turn | Demand Flows Total HV veh/h |  | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective Stop Rate | Aver. No. Average Cycles Speed km/h |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Vehicles veh |  |  | Distance m |  |  |  |  |
| SouthEast: Wallamore Road (SE) 0 |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 | L2 | 148 | 20.6 |  | 0.092 | 7.9 | LOS A | 0.0 | 0.0 | 0.00 | 0.59 | 0.00 | 60.2 |
| 22 | T1 | 21 | 30.0 | 0.013 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 80.0 |
| Appr |  | 169 | 21.7 | 0.092 | 6.9 | NA | 0.0 | 0.0 | 0.00 | 0.52 | 0.00 | 62.1 |
| NorthWest: Wallamore Road (NW) |  |  |  |  |  |  |  |  |  |  |  |  |
| 28 | T1 | 53 | 18.0 | 0.030 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 80.0 |
| 29 | R2 | 12 | 18.2 | 0.011 | 7.8 | LOS A | 0.0 | 0.3 | 0.30 | 0.60 | 0.30 | 58.3 |
| Appr |  | 64 | 18.0 | 0.030 | 1.4 | NA | 0.0 | 0.3 | 0.05 | 0.11 | 0.05 | 75.0 |
| SouthWest: Goddard Lane |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 | L2 | 7 | 57.1 | 0.182 | 8.6 | LOS A | 0.8 | 6.3 | 0.30 | 0.64 | 0.30 | 51.0 |
| 32 | R2 | 140 | 16.5 | 0.182 | 8.7 | LOS A | 0.8 | 6.3 | 0.30 | 0.64 | 0.30 | 58.5 |
| Appr |  | 147 | 18.6 | 0.182 | 8.7 | LOS A | 0.8 | 6.3 | 0.30 | 0.64 | 0.30 | 58.1 |
| All V | icles | 381 | 19.9 | 0.182 | 6.7 | NA | 0.8 | 6.3 | 0.12 | 0.50 | 0.12 | 62.2 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Project: E:ITTPP Projects Local CopylSidral18089\18089_181003_Oakburn Processing Plant.sip8

## MOVEMENT SUMMARY

## $\nabla$ Site: 101 [PM Growth Goddard - Armstrong]

Goddard Lane and Armstrong Street
PM Peak with Growth
$3: 15 \mathrm{pm}$ to $4: 15 \mathrm{pm}$ background + growth
Site Category: (None)
Giveway / Yield (Two-Way)

Movement Performance - Vehicles

| Mov | Turn | Demand | lows | Deg. | Average | Level of | 95\% Back | of Queue | Prop. | Effective | Aver. No. | Average |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ID |  | Total veh/h | $\begin{gathered} \text { HV } \\ \% \end{gathered}$ | Satn v/c | Delay sec | Service | Vehicles veh | Distance m | Queued | Stop Rate | Cycles | Speed km/h |
| NorthEast: Goddard Lane (north-east) |  |  |  |  |  |  |  |  |  |  |  |  |
| 25 | T1 | 168 | 5.0 | 0.108 | 0.2 | LOS A | 0.2 | 1.4 | 0.09 | 0.06 | 0.09 | 77.7 |
| 26 | R2 | 18 | 47.1 | 0.108 | 8.7 | LOS A | 0.2 | 1.4 | 0.09 | 0.06 | 0.09 | 58.1 |
| Approach |  | 186 | 9.0 | 0.108 | 1.0 | NA | 0.2 | 1.4 | 0.09 | 0.06 | 0.09 | 74.1 |
| NorthWest: Armstrong Street |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 | L2 | 27 | 34.6 | 0.129 | 5.2 | LOS A | 0.5 | 3.6 | 0.28 | 0.60 | 0.28 | 46.3 |
| 29 | R2 | 96 | 8.8 | 0.129 | 6.2 | LOS A | 0.5 | 3.6 | 0.28 | 0.60 | 0.28 | 33.3 |
| Approach |  | 123 | 14.5 | 0.129 | 6.0 | LOS A | 0.5 | 3.6 | 0.28 | 0.60 | 0.28 | 36.6 |
| SouthWest: Goddard Lane (south-west) |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 | L2 | 120 | 7.9 | 0.114 | 5.7 | LOS A | 0.0 | 0.0 | 0.00 | 0.38 | 0.00 | 60.2 |
| 31 | T1 | 79 | 20.0 | 0.114 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.38 | 0.00 | 70.8 |
| Appr |  | 199 | 12.7 | 0.114 | 3.4 | NA | 0.0 | 0.0 | 0.00 | 0.38 | 0.00 | 64.0 |
| All V | icles | 508 | 11.8 | 0.129 | 3.2 | NA | 0.5 | 3.6 | 0.10 | 0.32 | 0.10 | 55.9 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## $\theta$ Site: 101 [PM Growth Oxley - Duri]

Oxley Highway and Duri Road
PM Peak with Growth
3:15pm to 4:15pm background + growth
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Demand Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| NorthEast: Oxley Highway (NE) |  |  |  |  |  |  |  |  |  |  |  |  |
| 25 | T1 | 404 | 3.9 | 0.205 | 4.7 | LOS A | 0.0 | 0.0 | 0.00 | 0.46 | 0.00 | 55.5 |
| 26a | R1 | 409 | 6.9 | 0.387 | 9.8 | LOS A | 2.8 | 20.6 | 0.68 | 0.75 | 0.68 | 50.7 |
| Appr |  | 814 | 5.4 | 0.387 | 7.3 | LOS A | 2.8 | 20.6 | 0.34 | 0.61 | 0.34 | 53.0 |
| West: Oxley Highway (W) |  |  |  |  |  |  |  |  |  |  |  |  |
| 10a | L1 | 404 | 4.4 | 0.210 | 4.3 | LOS A | 0.0 | 0.0 | 0.00 | 0.47 | 0.00 | 55.5 |
| 12b | R3 | 408 | 8.8 | 0.352 | 10.8 | LOSA | 2.5 | 18.6 | 0.57 | 0.71 | 0.57 | 50.4 |
| Appr |  | 813 | 6.6 | 0.352 | 7.6 | LOS A | 2.5 | 18.6 | 0.29 | 0.59 | 0.29 | 52.8 |
| SouthWest: Duri Road |  |  |  |  |  |  |  |  |  |  |  |  |
| 30b | L3 | 295 | 11.4 | 0.188 | 4.2 | LOS A | 0.0 | 0.0 | 0.00 | 0.52 | 0.00 | 54.6 |
| 31 | T1 | 289 | 4.0 | 0.276 | 6.8 | LOS A | 1.9 | 13.5 | 0.64 | 0.66 | 0.64 | 52.8 |
| Approach |  | 584 | 7.7 | 0.276 | 5.5 | LOS A | 1.9 | 13.5 | 0.32 | 0.59 | 0.32 | 53.7 |
| All Vehicles |  | 2211 | 6.5 | 0.387 | 6.9 | LOS A | 2.8 | 20.6 | 0.31 | 0.60 | 0.31 | 53.1 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## $\nabla$ Site: 101 [PM Growth Oxley - Goddard]

Oxley Hwy and Goddard Ln
PM Peak with Growth
3:15pm to 4:15pm background + growth
Site Category: (None)
Giveway / Yield (Two-Way)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | Demand <br> Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| SouthEast: Oxley Highway (south-east) sec |  |  |  |  |  |  |  |  |  |  |  |
| 22 T1 | 152 | 17.4 | 0.087 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 100.0 |
| 23 R2 | 137 | 9.2 | 0.131 | 9.4 | LOS A | 0.5 | 4.1 | 0.38 | 0.67 | 0.38 | 64.8 |
| Approach | 288 | 13.5 | 0.131 | 4.4 | NA | 0.5 | 4.1 | 0.18 | 0.32 | 0.18 | 79.5 |
| NorthEast: Goddard Lane |  |  |  |  |  |  |  |  |  |  |  |
| 24 L2 | 178 | 5.9 | 0.320 | 8.7 | LOS A | 1.4 | 10.5 | 0.43 | 0.69 | 0.44 | 64.5 |
| 26 R2 | 79 | 5.3 | 0.320 | 13.5 | LOSA | 1.4 | 10.5 | 0.43 | 0.69 | 0.44 | 64.0 |
| Approach | 257 | 5.7 | 0.320 | 10.2 | LOS A | 1.4 | 10.5 | 0.43 | 0.69 | 0.44 | 64.3 |
| NorthWest: Oxley Highway (north-west) |  |  |  |  |  |  |  |  |  |  |  |
| 27 L2 | 61 | 17.2 | 0.037 | 9.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.63 | 0.00 | 69.1 |
| 28 T1 | 185 | 17.0 | 0.106 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 99.9 |
| Approach | 246 | 17.1 | 0.106 | 2.3 | NA | 0.0 | 0.0 | 0.00 | 0.16 | 0.00 | 89.9 |
| All Vehicles | 792 | 12.1 | 0.320 | 5.6 | NA | 1.4 | 10.5 | 0.21 | 0.39 | 0.21 | 76.4 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## Site: 101 [PM Growth Oxley - Marius - Brisbane ]

Oxley Highway, Marius Street and Brisbane Street
PM Peak Hour with Growth
3:00pm to 4:00pm background + growth
Site Category: (None)
Signals - Fixed Time Isolated Cycle Time $=114$ seconds (Site User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Turn | Demand Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \end{aligned}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| SouthEast: Marius Street (SE) |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 | L2 | 348 | 9.7 | 0.301 | 14.0 | LOS A | 7.9 | 60.1 | 0.45 | 0.71 | 0.45 | 39.8 |
| 22 | T1 | 542 | 4.5 | 0.737 | 27.8 | LOS B | 23.9 | 173.9 | 0.86 | 0.76 | 0.86 | 38.8 |
| 23 | R2 | 79 | 6.7 | 0.308 | 38.5 | LOS C | 3.4 | 25.4 | 0.80 | 0.77 | 0.80 | 33.4 |
| Appr | ach | 969 | 6.5 | 0.737 | 23.7 | LOS B | 23.9 | 173.9 | 0.71 | 0.74 | 0.71 | 38.5 |
| NorthEast: Brisbane Street |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 | L2 | 103 | 2.0 | 0.559 | 47.4 | LOS D | 10.7 | 77.2 | 0.93 | 0.79 | 0.93 | 31.4 |
| 25 | T1 | 280 | 6.0 | 0.559 | 41.8 | LOS C | 10.7 | 77.2 | 0.93 | 0.78 | 0.93 | 29.9 |
| 26 | R2 | 49 | 4.3 | 0.559 | 47.4 | LOS D | 10.6 | 77.8 | 0.92 | 0.78 | 0.92 | 34.6 |
| Appr | ach | 433 | 4.9 | 0.559 | 43.8 | LOS D | 10.7 | 77.8 | 0.93 | 0.79 | 0.93 | 30.9 |
| NorthWest: Marius Street (NW) |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 | L2 | 69 | 9.1 | 0.418 | 29.5 | LOS C | 12.8 | 92.9 | 0.74 | 0.67 | 0.74 | 41.6 |
| 28 | T1 | 560 | 3.2 | 0.418 | 23.6 | LOS B | 12.8 | 92.9 | 0.73 | 0.64 | 0.73 | 40.7 |
| 29 | R2 | 75 | 0.0 | 0.492 | 51.7 | LOS D | 3.9 | 27.4 | 0.93 | 0.79 | 0.93 | 26.9 |
| Appr | ach | 704 | 3.4 | 0.492 | 27.1 | LOS B | 12.8 | 92.9 | 0.75 | 0.66 | 0.75 | 39.0 |
| SouthWest: Oxley Highway |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 | L2 | 67 | 0.0 | 0.197 | 48.3 | LOS D | 3.2 | 22.4 | 0.89 | 0.75 | 0.89 | 27.8 |
| 31 | T1 | 198 | 8.5 | 0.643 | 46.8 | LOS D | 10.3 | 77.2 | 0.97 | 0.80 | 0.97 | 28.9 |
| 32 | R2 | 281 | 8.2 | 0.870 | 64.8 | LOS E | 17.5 | 130.8 | 1.00 | 0.96 | 1.27 | 20.0 |
| Approach |  | 546 | 7.3 | 0.870 | 56.3 | LOS D | 17.5 | 130.8 | 0.97 | 0.88 | 1.12 | 24.0 |
| All V | icles | 2653 | 5.6 | 0.870 | 34.6 | LOS C | 23.9 | 173.9 | 0.81 | 0.76 | 0.84 | 33.7 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## $\theta$ Site: 101 [PM Growth Peel - Jewry]

Peel Street and Jewry Street
PM Peak Hour with Growth
15:45am to 16:45am background + growth
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Turn | Deman <br> Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \hline \end{aligned}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| SouthEast: Peel Street (SE) min |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 | L2 | 361 | 8.2 | 0.878 | 41.3 | LOS C | 13.5 | 100.8 | 1.00 | 1.44 | 2.17 | 35.0 |
| 22 | T1 | 511 | 4.1 | 1.009 | 78.7 | LOS F | 32.5 | 235.5 | 1.00 | 2.10 | 3.81 | 26.3 |
| 23 | R2 | 12 | 0.0 | 1.009 | 82.5 | LOS F | 32.5 | 235.5 | 1.00 | 2.10 | 3.81 | 19.1 |
| Appro | ach | 883 | 5.7 | 1.009 | 63.5 | LOS E | 32.5 | 235.5 | 1.00 | 1.83 | 3.14 | 29.1 |
| NorthEast: Car Park |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 | L2 | 29 | 0.0 | 0.237 | 13.2 | LOS A | 1.2 | 8.2 | 0.87 | 0.87 | 0.87 | 26.5 |
| 25 | T1 | 21 | 0.0 | 0.237 | 13.2 | LOS A | 1.2 | 8.2 | 0.87 | 0.87 | 0.87 | 26.6 |
| 26 | R2 | 4 | 0.0 | 0.237 | 13.2 | LOS A | 1.2 | 8.2 | 0.87 | 0.87 | 0.87 | 26.8 |
| Appro | ach | 55 | 0.0 | 0.237 | 13.2 | LOS A | 1.2 | 8.2 | 0.87 | 0.87 | 0.87 | 26.6 |
| NorthWest: Peel Street (NW) |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 | L2 | 17 | 0.0 | 0.663 | 13.7 | LOS A | 7.0 | 50.2 | 0.94 | 1.05 | 1.22 | 27.3 |
| 28 | T1 | 418 | 3.5 | 0.663 | 13.5 | LOS A | 7.0 | 50.2 | 0.94 | 1.05 | 1.22 | 49.0 |
| 29 | R2 | 818 | 5.4 | 0.989 | 50.1 | LOS D | 36.5 | 267.0 | 1.00 | 1.80 | 3.13 | 33.0 |
| Appro | ach | 1253 | 4.7 | 0.989 | 37.4 | LOS C | 36.5 | 267.0 | 0.98 | 1.54 | 2.47 | 36.9 |
| SouthWest: Jewry Street |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 | L2 | 963 | 2.6 | 1.154 | 160.7 | LOS F | 104.8 | 749.8 | 1.00 | 4.01 | 7.98 | 16.2 |
| 31 | T1 | 24 | 8.7 | 0.796 | 21.2 | LOS B | 11.0 | 80.1 | 1.00 | 1.21 | 1.55 | 25.8 |
| 32 | R2 | 485 | 4.3 | 0.796 | 22.5 | LOS B | 11.0 | 80.1 | 1.00 | 1.21 | 1.55 | 43.7 |
| Approach |  | 1473 | 3.3 | 1.154 | 112.9 | LOS F | 104.8 | 749.8 | 1.00 | 3.04 | 5.75 | 20.7 |
| All Ve | hicles | 3663 | 4.3 | 1.154 | 73.7 | LOS F | 104.8 | 749.8 | 0.99 | 2.20 | 3.93 | 26.7 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

$\nabla$ Site: 101 [PM Growth Wallamore - Goddard ]
Wallamore Road and Goddard Lane
PM Peak with Growth
3:30pm to 4:30pm background + growth
Site Category: (None)
Giveway / Yield (Two-Way)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Deman <br> Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | $\begin{aligned} & \text { Deg. } \\ & \text { Satn } \\ & \text { v/c } \end{aligned}$ | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average <br> Speed km/h |
| SouthEast: Wallamore Road (SE) |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 | L2 | 249 | 7.2 | 0.141 | 7.7 | LOS A | 0.0 | 0.0 | 0.00 | 0.60 | 0.00 | 64.0 |
| 22 | T1 | 53 | 16.0 | 0.030 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 80.0 |
| Appr |  | 302 | 8.7 | 0.141 | 6.3 | NA | 0.0 | 0.0 | 0.00 | 0.49 | 0.00 | 66.3 |
| NorthWest: Wallamore Road (NW) |  |  |  |  |  |  |  |  |  |  |  |  |
| 28 | T1 | 28 | 14.8 | 0.016 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 80.0 |
| 29 | R2 | 7 | 57.1 | 0.010 | 9.9 | LOS A | 0.0 | 0.4 | 0.43 | 0.64 | 0.43 | 48.2 |
| Appr |  | 36 | 23.5 | 0.016 | 2.0 | NA | 0.0 | 0.4 | 0.09 | 0.13 | 0.09 | 70.4 |
| SouthWest: Goddard Lane |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 | L2 | 15 | 0.0 | 0.350 | 7.9 | LOS A | 1.7 | 12.9 | 0.42 | 0.69 | 0.43 | 64.3 |
| 32 | R2 | 266 | 7.9 | 0.350 | 9.3 | LOS A | 1.7 | 12.9 | 0.42 | 0.69 | 0.43 | 60.3 |
| Approach |  | 281 | 7.5 | 0.350 | 9.2 | LOS A | 1.7 | 12.9 | 0.42 | 0.69 | 0.43 | 60.5 |
| All Vehicles |  | 619 | 9.0 | 0.350 | 7.4 | NA | 1.7 | 12.9 | 0.20 | 0.56 | 0.20 | 63.8 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## $\nabla$ Site: 101 [AM PP Growth Goddard - Armstrong]

Goddard Lane and Armstrong Street
AM Peak with Processing Plant and Growth
7:45am to 8:45am background $+6-7$ am plant traffic + growth
Site Category: (None)
Giveway / Yield (Two-Way)

Movement Performance - Vehicles

| Mov ID |  | Demand <br> Total veh/h | Flows <br> HV <br> \% | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| NorthEast: Goddard Lane (north-east) |  |  |  |  |  |  |  |  |  |  |  |  |
| 25 | T1 | 81 | 22.1 | 0.090 | 0.6 | LOS A | 0.4 | 3.0 | 0.28 | 0.26 | 0.28 | 70.0 |
| 26 | R2 | 55 | 17.3 | 0.090 | 7.9 | LOS A | 0.4 | 3.0 | 0.28 | 0.26 | 0.28 | 56.1 |
| Appr |  | 136 | 20.2 | 0.090 | 3.6 | NA | 0.4 | 3.0 | 0.28 | 0.26 | 0.28 | 61.9 |
| NorthWest: Armstrong Street |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 | L2 | 16 | 40.0 | 0.090 | 5.4 | LOS A | 0.3 | 3.1 | 0.33 | 0.61 | 0.33 | 45.1 |
| 29 | R2 | 54 | 52.9 | 0.090 | 7.2 | LOS A | 0.3 | 3.1 | 0.33 | 0.61 | 0.33 | 31.9 |
| Approach |  | 69 | 50.0 | 0.090 | 6.8 | LOS A | 0.3 | 3.1 | 0.33 | 0.61 | 0.33 | 35.3 |
| SouthWest: Goddard Lane (south-west) |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 | L2 | 109 | 21.2 | 0.130 | 5.7 | LOS A | 0.0 | 0.0 | 0.00 | 0.30 | 0.00 | 56.0 |
| 31 | T1 | 117 | 5.4 | 0.130 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.30 | 0.00 | 73.4 |
| Appr |  | 226 | 13.0 | 0.130 | 2.7 | NA | 0.0 | 0.0 | 0.00 | 0.30 | 0.00 | 63.8 |
| All V | icles | 432 | 21.2 | 0.130 | 3.7 | NA | 0.4 | 3.1 | 0.14 | 0.34 | 0.14 | 55.7 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## $\theta$ Site: 101 [AM PP Growth Oxley - Duri]

Oxley Highway and Duri Road
AM Peak with Processing Plant and Growth
8:00am to 9:00am background +6 -7am plant traffic + growth
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Turn | Deman <br> Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| NorthEast: Oxley Highway (NE) |  |  |  |  |  |  |  |  |  |  |  |  |
| 25 | T1 | 193 | 6.0 | 0.099 | 4.7 | LOS A | 0.0 | 0.0 | 0.00 | 0.46 | 0.00 | 55.5 |
| 26a | R1 | 335 | 4.7 | 0.287 | 8.9 | LOS A | 2.0 | 14.3 | 0.56 | 0.68 | 0.56 | 51.1 |
| Appr | ach | 527 | 5.2 | 0.287 | 7.3 | LOS A | 2.0 | 14.3 | 0.35 | 0.60 | 0.35 | 52.6 |
| West: Oxley Highway (W) |  |  |  |  |  |  |  |  |  |  |  |  |
| 10a | L1 | 336 | 5.3 | 0.176 | 4.3 | LOS A | 0.0 | 0.0 | 0.00 | 0.47 | 0.00 | 55.5 |
| 12b | R3 | 285 | 13.7 | 0.311 | 12.3 | LOS A | 2.2 | 16.9 | 0.72 | 0.79 | 0.72 | 49.7 |
| Appr |  | 621 | 9.2 | 0.311 | 8.0 | LOS A | 2.2 | 16.9 | 0.33 | 0.62 | 0.33 | 52.6 |
| SouthWest: Duri Road |  |  |  |  |  |  |  |  |  |  |  |  |
| 30b | L3 | 346 | 14.0 | 0.224 | 4.2 | LOS A | 0.0 | 0.0 | 0.00 | 0.52 | 0.00 | 54.5 |
| 31 | T1 | 522 | 3.6 | 0.456 | 6.7 | LOS A | 3.5 | 25.0 | 0.65 | 0.66 | 0.65 | 52.8 |
| Approach |  | 868 | 7.8 | 0.456 | 5.7 | LOS A | 3.5 | 25.0 | 0.39 | 0.61 | 0.39 | 53.4 |
| All Vehicles |  | 2017 | 7.5 | 0.456 | 6.8 | LOS A | 3.5 | 25.0 | 0.36 | 0.61 | 0.36 | 53.0 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## MOVEMENT SUMMARY

## $\nabla$ Site: 101 [AM PP Growth Oxley - Goddard]

Oxley Hwy and Goddard Ln
AM Peak with Processing Plant and Growth
7:45am to 8:45am background $+6-7$ am plant traffic + growth
Site Category: (None)
Giveway / Yield (Two-Way)

Movement Performance - Vehicles


Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## Site: 101 [AM PP Growth Oxley - Marius - Brisbane]

Oxley Highway, Marius Street and Brisbane Street
AM Peak Hour with Processing Plant and Growth
8:15am to 9:15am background $+6-7 \mathrm{am}$ plant traffic + growth
Site Category: (None)
Signals - Fixed Time Isolated Cycle Time $=93$ seconds (Site User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Demand <br> Total <br> veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| SouthEast: Marius Street (SE) |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 | L2 | 276 | 7.3 | 0.238 | 12.5 | LOS A | 5.0 | 37.4 | 0.44 | 0.70 | 0.44 | 41.2 |
| 22 | T1 | 533 | 6.5 | 0.862 | 39.0 | LOS C | 25.9 | 191.4 | 0.98 | 1.01 | 1.18 | 34.0 |
| 23 | R2 | 44 | 4.8 | 0.206 | 38.5 | LOS C | 1.7 | 12.4 | 0.85 | 0.74 | 0.85 | 33.4 |
| Appr | ach | 853 | 6.7 | 0.862 | 30.4 | LOS C | 25.9 | 191.4 | 0.80 | 0.90 | 0.92 | 35.4 |
| NorthEast: Brisbane Street |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 | L2 | 126 | 3.3 | 0.594 | 41.8 | LOS C | 9.8 | 71.7 | 0.95 | 0.81 | 0.95 | 33.2 |
| 25 | T1 | 291 | 8.0 | 0.594 | 36.2 | LOS C | 9.8 | 71.7 | 0.95 | 0.80 | 0.95 | 32.0 |
| 26 | R2 | 51 | 4.2 | 0.594 | 41.7 | LOS C | 9.7 | 72.4 | 0.95 | 0.80 | 0.95 | 36.5 |
| Appr | ach | 467 | 6.3 | 0.594 | 38.3 | LOS C | 9.8 | 72.4 | 0.95 | 0.80 | 0.95 | 32.9 |
| NorthWest: Marius Street (NW) |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 | L2 | 68 | 0.0 | 0.490 | 31.2 | LOS C | 11.0 | 82.1 | 0.83 | 0.73 | 0.83 | 40.8 |
| 28 | T1 | 522 | 10.1 | 0.490 | 25.6 | LOS B | 11.0 | 82.1 | 0.83 | 0.71 | 0.83 | 39.6 |
| 29 | R2 | 51 | 0.0 | 0.452 | 52.8 | LOS D | 2.4 | 16.6 | 0.99 | 0.75 | 0.99 | 26.6 |
| Appr | ach | 641 | 8.2 | 0.490 | 28.4 | LOS B | 11.0 | 82.1 | 0.84 | 0.72 | 0.84 | 38.5 |
| SouthWest: Oxley Highway |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 | L2 | 53 | 4.0 | 0.118 | 35.0 | LOS C | 1.9 | 13.5 | 0.81 | 0.73 | 0.81 | 32.4 |
| 31 | T1 | 199 | 2.1 | 0.421 | 32.1 | LOS C | 7.7 | 54.7 | 0.89 | 0.73 | 0.89 | 34.5 |
| 32 | R2 | 234 | 11.7 | 0.551 | 39.2 | LOS C | 9.4 | 72.7 | 0.92 | 0.82 | 0.92 | 26.8 |
| Approach |  | 485 | 6.9 | 0.551 | 35.8 | LOS C | 9.4 | 72.7 | 0.90 | 0.77 | 0.90 | 30.6 |
| All V | icles | 2446 | 7.1 | 0.862 | 32.4 | LOS C | 25.9 | 191.4 | 0.86 | 0.81 | 0.90 | 34.8 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## Site: 101 [AM PP Growth Peel - Jewry]

Peel Street and Jewry Street
AM Peak Hour with Processing Plant and Growth
8:15am to 9:15am + 6-7am plant traffic + growth
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Turn | Deman <br> Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| SouthEast: Peel Street (SE) din |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 | L2 | 382 | 9.6 | 0.798 | 28.2 | LOS B | 10.8 | 82.2 | 1.00 | 1.30 | 1.75 | 40.0 |
| 22 | T1 | 354 | 5.4 | 0.839 | 34.6 | LOS C | 11.8 | 86.5 | 1.00 | 1.36 | 1.94 | 38.3 |
| 23 | R2 | 5 | 0.0 | 0.839 | 38.3 | LOS C | 11.8 | 86.5 | 1.00 | 1.36 | 1.94 | 24.7 |
| Appr | ach | 741 | 7.5 | 0.839 | 31.3 | LOS C | 11.8 | 86.5 | 1.00 | 1.32 | 1.84 | 39.0 |
| NorthEast: Car Park |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 | L2 | 17 | 0.0 | 0.152 | 15.0 | LOS B | 0.7 | 5.2 | 0.88 | 0.88 | 0.88 | 26.1 |
| 25 | T1 | 12 | 0.0 | 0.152 | 15.0 | LOS B | 0.7 | 5.2 | 0.88 | 0.88 | 0.88 | 26.3 |
| 26 | R2 | 1 | 0.0 | 0.152 | 15.0 | LOS B | 0.7 | 5.2 | 0.88 | 0.88 | 0.88 | 26.5 |
| Appr | ach | 29 | 0.0 | 0.152 | 15.0 | LOS B | 0.7 | 5.2 | 0.88 | 0.88 | 0.88 | 26.2 |
| NorthWest: Peel Street (NW) |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 | L2 | 17 | 12.5 | 0.708 | 13.8 | LOS A | 8.3 | 60.3 | 0.93 | 1.02 | 1.21 | 27.4 |
| 28 | T1 | 631 | 3.8 | 1.014 | 20.0 | LOS B | 48.3 | 354.0 | 0.94 | 1.18 | 1.61 | 44.8 |
| 29 | R2 | 855 | 5.7 | 1.014 | 57.3 | LOS E | 48.3 | 354.0 | 1.00 | 1.96 | 3.52 | 31.1 |
| Appr |  | 1502 | 5.0 | 1.014 | 41.1 | LOS C | 48.3 | 354.0 | 0.97 | 1.62 | 2.70 | 35.6 |
| SouthWest: Jewry Street |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 | L2 | 723 | 6.0 | 0.737 | 10.5 | LOS A | 10.0 | 73.4 | 0.94 | 0.91 | 1.14 | 49.8 |
| 31 | T1 | 21 | 10.0 | 0.540 | 11.1 | LOS A | 4.6 | 35.1 | 0.79 | 0.85 | 0.86 | 27.7 |
| 32 | R2 | 394 | 10.4 | 0.540 | 12.7 | LOS A | 4.6 | 35.1 | 0.79 | 0.85 | 0.86 | 49.3 |
| Approach |  | 1138 | 7.6 | 0.737 | 11.3 | LOS A | 10.0 | 73.4 | 0.89 | 0.89 | 1.04 | 48.9 |
| All V | icles | 3411 | 6.4 | 1.014 | 28.8 | LOS C | 48.3 | 354.0 | 0.95 | 1.31 | 1.94 | 39.8 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## $\nabla$ Site: 101 [AM PP Growth Wallamore - Goddard]

Wallamore Road and Goddard Lane
AM Peak with Processing Plant and Growth
8:00am to 9:00am background $+6-7$ am plant traffic + growth
Site Category: (None)
Giveway / Yield (Two-Way)

Movement Performance - Vehicles


Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## $\nabla$ site: 101 [PM PP Growth Goddard - Armstrong]

Goddard Lane and Armstrong Street
PM Peak with Processing Plant with Growth
$3: 15 \mathrm{pm}$ to $4: 15 \mathrm{pm}$ background $+3-4 \mathrm{pm}$ plant traffic + growth
Site Category: (None)
Giveway / Yield (Two-Way)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{ll} \text { Mov Turn } \\ \text { ID } \end{array}$ | Deman <br> Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| NorthEast: Goddard Lane (north-east) |  |  |  |  |  |  |  |  |  |  |  |
| 25 T1 | 168 | 5.0 | 0.108 | 0.2 | LOS A | 0.2 | 1.4 | 0.10 | 0.06 | 0.10 | 77.7 |
| 26 R2 | 18 | 47.1 | 0.108 | 8.8 | LOS A | 0.2 | 1.4 | 0.10 | 0.06 | 0.10 | 58.1 |
| Approach | 186 | 9.0 | 0.108 | 1.0 | NA | 0.2 | 1.4 | 0.10 | 0.06 | 0.10 | 74.0 |
| NorthWest: Armstrong Street |  |  |  |  |  |  |  |  |  |  |  |
| 27 L2 | 111 | 8.6 | 0.339 | 5.0 | LOS A | 1.5 | 11.0 | 0.30 | 0.61 | 0.30 | 51.1 |
| 29 R2 | 233 | 9.0 | 0.339 | 6.7 | LOS A | 1.5 | 11.0 | 0.30 | 0.61 | 0.30 | 33.3 |
| Approach | 343 | 8.9 | 0.339 | 6.2 | LOS A | 1.5 | 11.0 | 0.30 | 0.61 | 0.30 | 39.2 |
| SouthWest: Goddard Lane (south-west) |  |  |  |  |  |  |  |  |  |  |  |
| 30 L2 | 133 | 16.7 | 0.126 | 5.7 | LOS A | 0.0 | 0.0 | 0.00 | 0.39 | 0.00 | 56.3 |
| 31 T1 | 79 | 20.0 | 0.126 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.39 | 0.00 | 70.8 |
| Approach | 212 | 17.9 | 0.126 | 3.6 | NA | 0.0 | 0.0 | 0.00 | 0.39 | 0.00 | 61.0 |
| All Vehicles | 741 | 11.5 | 0.339 | 4.1 | NA | 1.5 | 11.0 | 0.16 | 0.41 | 0.16 | 49.3 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## $\theta$ Site: 101 [PM PP Growth Oxley - Duri]

Oxley Highway and Duri Road
PM Peak with Processing Plant and Growth
$3: 15 \mathrm{pm}$ to $4: 15 \mathrm{pm}$ background $+3-4 \mathrm{pm}$ plant traffic + growth
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Mov } \\ \text { ID } \end{gathered}$ | Turn | Deman <br> Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| NorthEast: Oxley Highway (NE) |  |  |  |  |  |  |  |  |  |  |  |  |
| 25 | T1 | 404 | 3.9 | 0.205 | 4.7 | LOS A | 0.0 | 0.0 | 0.00 | 0.46 | 0.00 | 55.5 |
| 26a | R1 | 412 | 7.4 | 0.412 | 10.3 | LOS A | 3.0 | 22.7 | 0.73 | 0.78 | 0.73 | 50.5 |
| Appr | ach | 816 | 5.7 | 0.412 | 7.5 | LOS A | 3.0 | 22.7 | 0.37 | 0.62 | 0.37 | 52.9 |
| West: Oxley Highway (W) |  |  |  |  |  |  |  |  |  |  |  |  |
| 10a | L1 | 462 | 4.1 | 0.240 | 4.3 | LOS A | 0.0 | 0.0 | 0.00 | 0.47 | 0.00 | 55.5 |
| 12b | R3 | 469 | 8.5 | 0.402 | 10.9 | LOSA | 3.0 | 22.3 | 0.60 | 0.71 | 0.60 | 50.3 |
| Appr |  | 932 | 6.3 | 0.402 | 7.6 | LOS A | 3.0 | 22.3 | 0.30 | 0.59 | 0.30 | 52.7 |
| SouthWest: Duri Road |  |  |  |  |  |  |  |  |  |  |  |  |
| 30b | L3 | 300 | 13.0 | 0.193 | 4.2 | LOS A | 0.0 | 0.0 | 0.00 | 0.52 | 0.00 | 54.5 |
| 31 | T1 | 289 | 4.0 | 0.278 | 6.8 | LOSA | 1.9 | 13.8 | 0.65 | 0.66 | 0.65 | 52.8 |
| Approach |  | 589 | 8.6 | 0.278 | 5.5 | LOS A | 1.9 | 13.8 | 0.32 | 0.59 | 0.32 | 53.7 |
| All Vehicles |  | 2337 | 6.7 | 0.412 | 7.0 | LOS A | 3.0 | 22.7 | 0.33 | 0.60 | 0.33 | 53.0 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## MOVEMENT SUMMARY

## $\nabla$ Site: 101 [PM PP Growth Oxley - Goddard]

Oxley Hwy and Goddard Ln
PM Peak with Processing Plant and Growth
$3: 15 \mathrm{pm}$ to $4: 15 \mathrm{pm}$ background $+3-4 \mathrm{pm}$ plant traffic + growth
Site Category: (None)
Giveway / Yield (Two-Way)


Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## Site: 101 [PM PP Growth Oxley - Marius - Brisbane]

Oxley Highway, Marius Street and Brisbane Street
PM Peak Hour with Processing Plant and Growth
3:00pm to $4: 00 \mathrm{pm}$ background $+3-4 \mathrm{pm}$ plant traffic + growth
Site Category: (None)
Signals - Fixed Time Isolated Cycle Time $=114$ seconds (Site User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Turn | Demand <br> Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| SouthEast: Marius Street (SE) |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 | L2 | 352 | 10.5 | 0.305 | 14.1 | LOS A | 8.0 | 61.3 | 0.45 | 0.71 | 0.45 | 39.7 |
| 22 | T1 | 542 | 4.5 | 0.737 | 27.8 | LOS B | 23.9 | 173.9 | 0.86 | 0.76 | 0.86 | 38.8 |
| 23 | R2 | 79 | 6.7 | 0.308 | 38.5 | LOS C | 3.4 | 25.4 | 0.80 | 0.77 | 0.80 | 33.4 |
| Appr |  | 973 | 6.8 | 0.737 | 23.7 | LOS B | 23.9 | 173.9 | 0.71 | 0.74 | 0.71 | 38.5 |
| NorthEast: Brisbane Street |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 | L2 | 103 | 2.0 | 0.559 | 47.4 | LOS D | 10.7 | 77.2 | 0.93 | 0.79 | 0.93 | 31.4 |
| 25 | T1 | 280 | 6.0 | 0.559 | 41.8 | LOS C | 10.7 | 77.2 | 0.93 | 0.78 | 0.93 | 29.9 |
| 26 | R2 | 49 | 4.3 | 0.559 | 47.4 | LOS D | 10.6 | 77.8 | 0.92 | 0.78 | 0.92 | 34.6 |
| Appr | ach | 433 | 4.9 | 0.559 | 43.8 | LOS D | 10.7 | 77.8 | 0.93 | 0.79 | 0.93 | 30.9 |
| NorthWest: Marius Street (NW) |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 | L2 | 69 | 9.1 | 0.418 | 29.5 | LOS C | 12.8 | 92.9 | 0.74 | 0.67 | 0.74 | 41.6 |
| 28 | T1 | 560 | 3.2 | 0.418 | 23.6 | LOS B | 12.8 | 92.9 | 0.73 | 0.64 | 0.73 | 40.7 |
| 29 | R2 | 75 | 0.0 | 0.494 | 51.7 | LOS D | 3.9 | 27.4 | 0.93 | 0.79 | 0.93 | 26.9 |
| Appr |  | 704 | 3.4 | 0.494 | 27.1 | LOS B | 12.8 | 92.9 | 0.75 | 0.66 | 0.75 | 39.0 |
| SouthWest: Oxley Highway |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 | L2 | 76 | 0.0 | 0.222 | 48.6 | LOS D | 3.6 | 25.4 | 0.89 | 0.76 | 0.89 | 27.7 |
| 31 | T1 | 214 | 7.9 | 0.707 | 48.3 | LOS D | 11.4 | 85.3 | 0.98 | 0.84 | 1.04 | 28.4 |
| 32 | R2 | 298 | 8.1 | 0.921 | 73.4 | LOS F | 20.1 | 150.3 | 1.00 | 1.02 | 1.41 | 18.4 |
| Approach |  | 587 | 7.0 | 0.921 | 61.1 | LOS E | 20.1 | 150.3 | 0.98 | 0.92 | 1.20 | 22.9 |
| All V | icles | 2697 | 5.7 | 0.921 | 36.0 | LOS C | 23.9 | 173.9 | 0.81 | 0.77 | 0.86 | 33.1 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## Site: 101 [PM PP Growth Peel - Jewry]

Peel Street and Jewry Street
PM Peak Hour with Processing Plant and Growth + growth
15:45am to 16:45am background $+3-4 \mathrm{pm}$ plant traffic
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Turn | Deman <br> Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \text { \% } \end{aligned}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed $\mathrm{km} / \mathrm{h}$ |
| SouthEast: Peel Street (SE) |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 | L2 | 361 | 8.2 | 0.857 | 36.7 | LOS C | 12.3 | 92.4 | 1.00 | 1.39 | 2.03 | 36.6 |
| 22 | T1 | 511 | 4.1 | 0.986 | 66.4 | LOS E | 28.4 | 205.9 | 1.00 | 1.95 | 3.40 | 28.8 |
| 23 | R2 | 12 | 0.0 | 0.986 | 70.2 | LOS E | 28.4 | 205.9 | 1.00 | 1.95 | 3.40 | 20.4 |
| Appr |  | 883 | 5.7 | 0.986 | 54.3 | LOS D | 28.4 | 205.9 | 1.00 | 1.72 | 2.84 | 31.3 |
| NorthEast: Car Park |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 | L2 | 29 | 0.0 | 0.242 | 13.6 | LOS A | 1.2 | 8.4 | 0.87 | 0.87 | 0.87 | 26.4 |
| 25 | T1 | 21 | 0.0 | 0.242 | 13.6 | LOS A | 1.2 | 8.4 | 0.87 | 0.87 | 0.87 | 26.5 |
| 26 | R2 | 4 | 0.0 | 0.242 | 13.7 | LOSA | 1.2 | 8.4 | 0.87 | 0.87 | 0.87 | 26.7 |
| Appr |  | 55 | 0.0 | 0.242 | 13.6 | LOS A | 1.2 | 8.4 | 0.87 | 0.87 | 0.87 | 26.5 |
| NorthWest: Peel Street (NW) |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 | L2 | 17 | 0.0 | 0.689 | 15.0 | LOS B | 7.6 | 54.6 | 0.97 | 1.10 | 1.30 | 27.0 |
| 28 | T1 | 418 | 3.5 | 0.689 | 14.9 | LOS B | 7.6 | 54.6 | 0.97 | 1.10 | 1.30 | 48.1 |
| 29 | R2 | 818 | 5.4 | 1.028 | 71.9 | LOS F | 47.7 | 349.4 | 1.00 | 2.22 | 4.14 | 27.7 |
| Appr |  | 1253 | 4.7 | 1.028 | 52.1 | LOS D | 47.7 | 349.4 | 0.99 | 1.83 | 3.15 | 32.2 |
| SouthWest: Jewry Street |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 | L2 | 985 | 2.6 | 1.176 | 179.3 | LOS F | 116.1 | 830.2 | 1.00 | 4.31 | 8.66 | 15.0 |
| 31 | T1 | 24 | 8.7 | 0.835 | 23.6 | LOS B | 13.0 | 94.6 | 1.00 | 1.26 | 1.68 | 25.4 |
| 32 | R2 | 519 | 4.1 | 0.835 | 24.9 | LOS B | 13.0 | 94.6 | 1.00 | 1.26 | 1.68 | 42.5 |
| Approach |  | 1528 | 3.2 | 1.176 | 124.4 | LOS F | 116.1 | 830.2 | 1.00 | 3.23 | 6.18 | 19.5 |
| All V | icles | 3719 | 4.2 | 1.176 | 81.8 | LOS F | 116.1 | 830.2 | 0.99 | 2.37 | 4.29 | 25.2 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## $\nabla$ Site: 101 [PM PP Growth Wallamore - Goddard]

Wallamore Road and Goddard Lane
PM Peak with Processing Plant and Growth
3:30pm to $4: 30 \mathrm{pm}$ background $+3-4 \mathrm{pm}$ plant traffic + growth
Site Category: (None)
Giveway / Yield (Two-Way)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{ll} \text { Mov Turn } \\ \text { ID } \end{array}$ | Deman Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | $\begin{aligned} & \text { Deg. } \\ & \text { Satn } \\ & \text { v/c } \end{aligned}$ | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| SouthEast: Wallamore Road (SE) |  |  |  |  |  |  |  |  |  |  |  |
| 21 L2 | 249 | 7.2 | 0.141 | 7.7 | LOS A | 0.0 | 0.0 | 0.00 | 0.60 | 0.00 | 64.0 |
| 22 T1 | 53 | 16.0 | 0.030 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 80.0 |
| Approach | 302 | 8.7 | 0.141 | 6.3 | NA | 0.0 | 0.0 | 0.00 | 0.49 | 0.00 | 66.3 |
| NorthWest: Wallamore Road (NW) |  |  |  |  |  |  |  |  |  |  |  |
| 28 T1 | 28 | 14.8 | 0.016 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 80.0 |
| 29 R2 | 7 | 57.1 | 0.010 | 9.9 | LOS A | 0.0 | 0.4 | 0.43 | 0.64 | 0.43 | 48.2 |
| Approach | 36 | 23.5 | 0.016 | 2.0 | NA | 0.0 | 0.4 | 0.09 | 0.13 | 0.09 | 70.4 |
| SouthWest: Goddard Lane |  |  |  |  |  |  |  |  |  |  |  |
| 30 L2 | 19 | 0.0 | 0.449 | 8.5 | LOS A | 3.0 | 22.3 | 0.46 | 0.73 | 0.54 | 63.5 |
| 32 R2 | 345 | 6.1 | 0.449 | 10.0 | LOS A | 3.0 | 22.3 | 0.46 | 0.73 | 0.54 | 60.1 |
| Approach | 364 | 5.8 | 0.449 | 9.9 | LOS A | 3.0 | 22.3 | 0.46 | 0.73 | 0.54 | 60.3 |
| All Vehicles | 702 | 7.9 | 0.449 | 8.0 | NA | 3.0 | 22.3 | 0.25 | 0.60 | 0.29 | 63.2 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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[^0]:    A The first vehicle identified in multiple vehicle crashes.

[^1]:    A The first vehicle identified in multiple vehicle crashes.

[^2]:    A The first vehicle identified in multiple vehicle crashes.

[^3]:    A The first vehicle identified in multiple vehicle crashes.

[^4]:    A The first vehicle identified in multiple vehicle crashes.

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